

# Thermo-Calc Software

Thermo-Calc: For All Kinds of Thermodynamic Calculations!

## Thermodynamic Calculations for Materials in Corrosive Environments

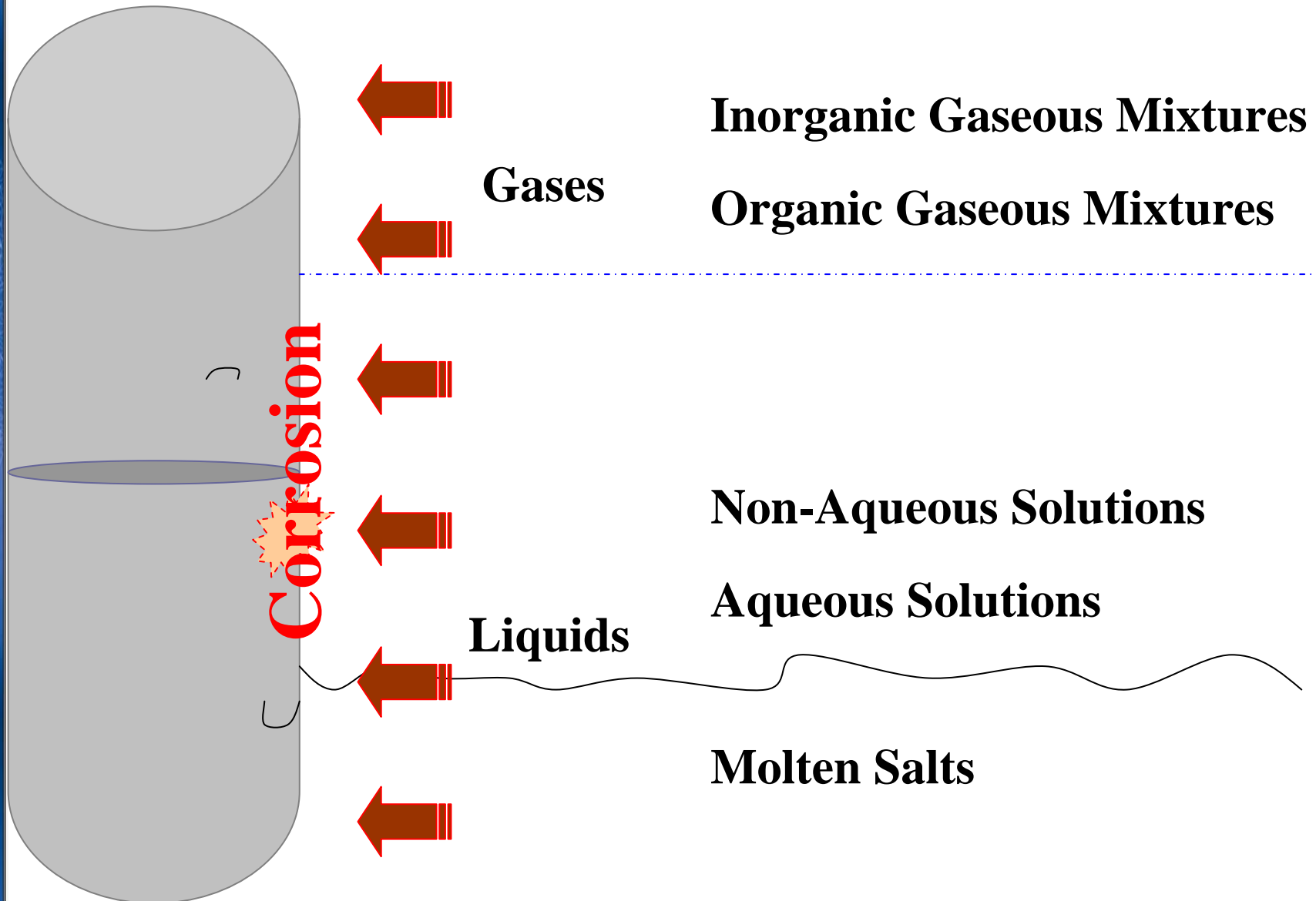
SINTEF, Trondheim, May 27, 2008

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# Application Environments



- Aqueous Corrosion; *Non-Aqueous Corrosion*
- Molten Salt Corrosion
- High-Temperature (Gaseous) Corrosion
- Surface Redox Reactions

# Aqueous Solution Models & Databases

Thermodynamic models handle EOS & all kinds of thermodynamic properties for various materials.

**Following models are now available in Thermo-Calc:**

Component-Energy Model (*interaction on up to ten sublattices*):

Redlich-Kister polynomials (Muggianu or Kohler extrapolation)

Stoichiometric constraints

Interstitial solution

Chemical ordering

Ionic constituents

Ionic Two-Sublattice Liquid Model

Associated Solutions

Quasi-chemical Model

Kapoor-Frohberg Cell Model

Magnetic Ordering

CVM (Cluster Variation Methods) for chemical ordering

Birch-Murnaghan Model (pressure dependency)

SUPERFLUID fluid & gaseous mixture

Aqueous Solution Models (DHLL, SIT, HKF & PITZ)

←-----→

*Databases:*

**TCAQ2 & AQS2**

Flory-Huggins Model for polymers

## *MSE R&D:*

- Hydro-Metallurgical Processes
- Hydrothermal Formation and Separation Processes
- High-/Low-Temperature Corrosion Processes
- Recycling Processes

## *Other R&D:*

- Aqueous Chemistry
- Chemical Engineering
- Food, Medicine & Energy Production
- Geochemical Systems (Natural Resources)
- Environmental Protections of Water Resources
- Environmental Impact of Nuclear Fuel Waste
- Environmental Assessment of Industrial Pollution
- ... *and many more*

# Properties in Aqueous-Involving Systems

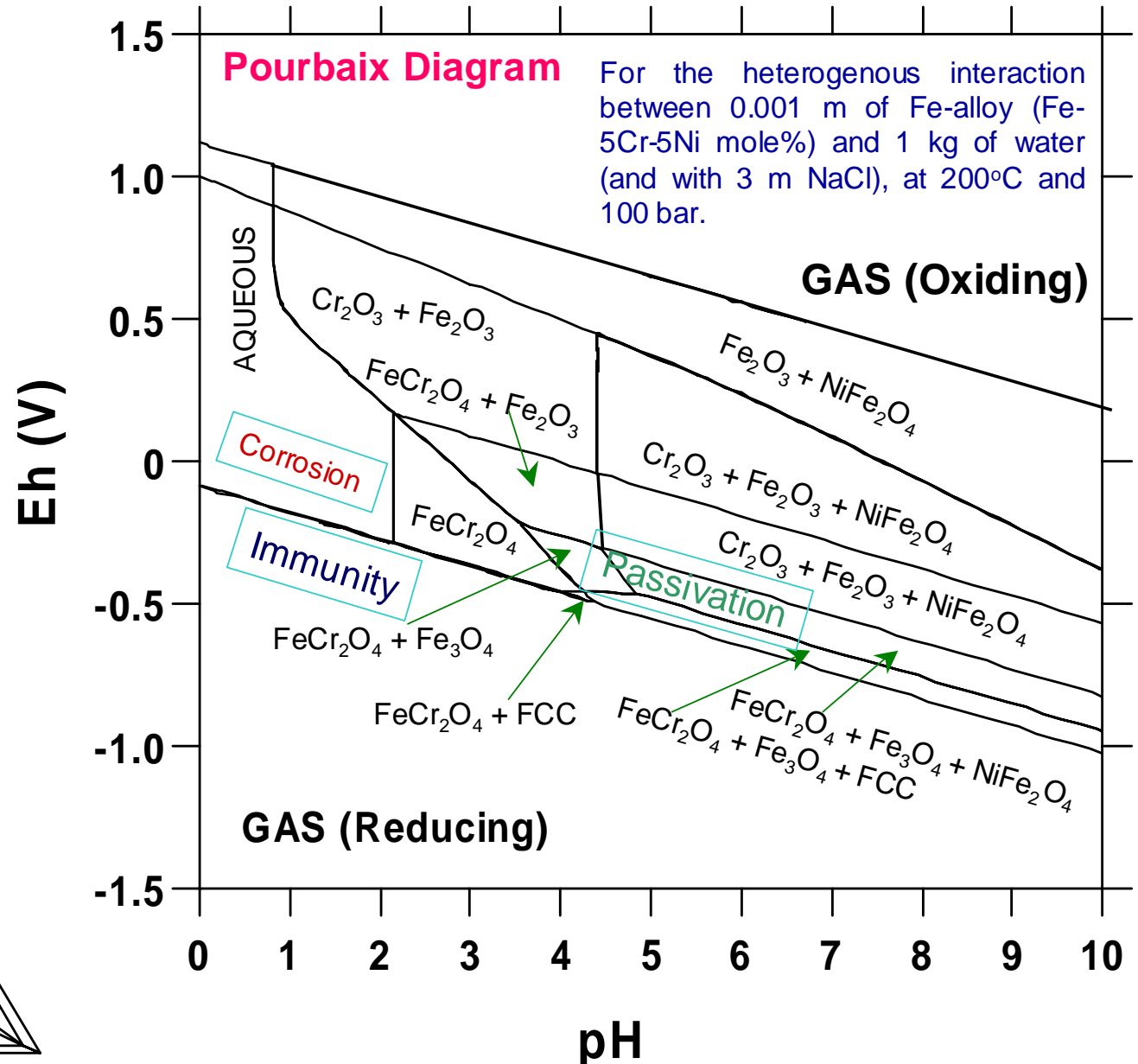
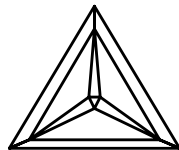
Use Thermo-Calc and Databases to Calculate Heterogeneous Equilibria and Phase/Property Diagrams Involving Aqueous Solutions with following outputs:

T	Temperature (°C or K)
P	Pressure (Pa)
NP	Stable Phase (mole/kg of water)
BP	Stable Phase (gram/kg of water)
pH	Acidity
Eh	Electronic Potential (V)
Ah	Electronic Affinity (kJ)
pe	Electronic Activity ( $\log_{10}ACRe$ )
IS	Ionic Strength
TM	Total Concentration (in molality)
Aw	Activity of Water
Oc	Osmotic Coefficient
MF(AQsp)	Mole Fractions of Aqueous Species
ML(AQsp)	Molalities of Aqueous Species
AI(AQsp)	Activities of Aqueous Species
RC(AQsp)	Activity Coefficients of Aqueous Species

*... and many more ...*

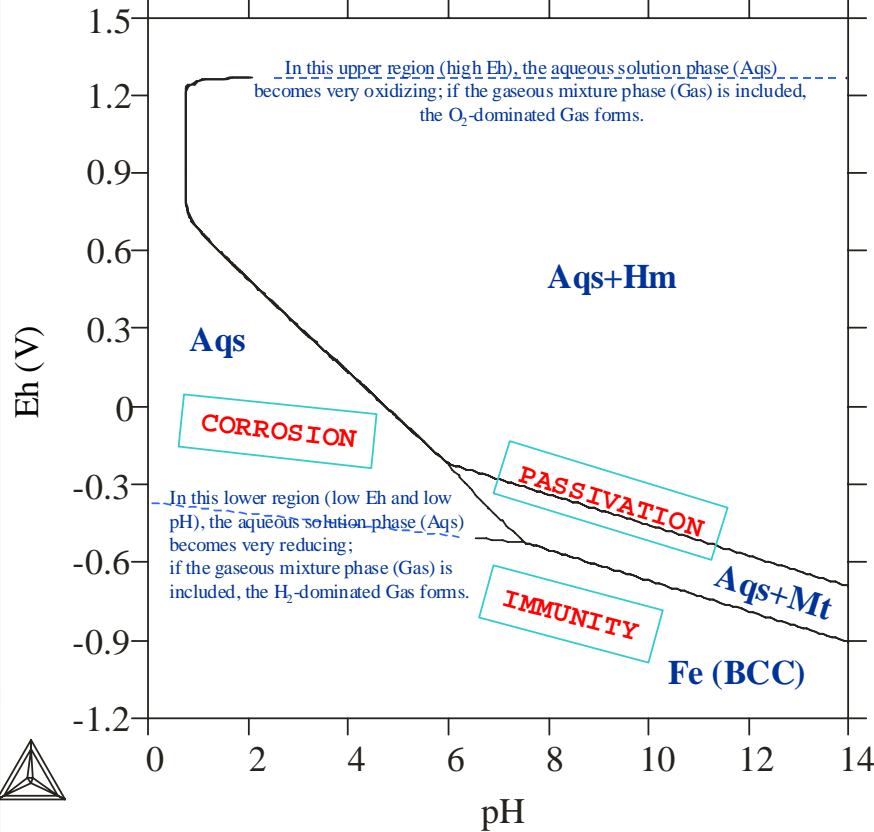
# Aqueous Corrosion: Pourbaix Diagrams

## Pourbaix Diagrams in Multicomponent Systems

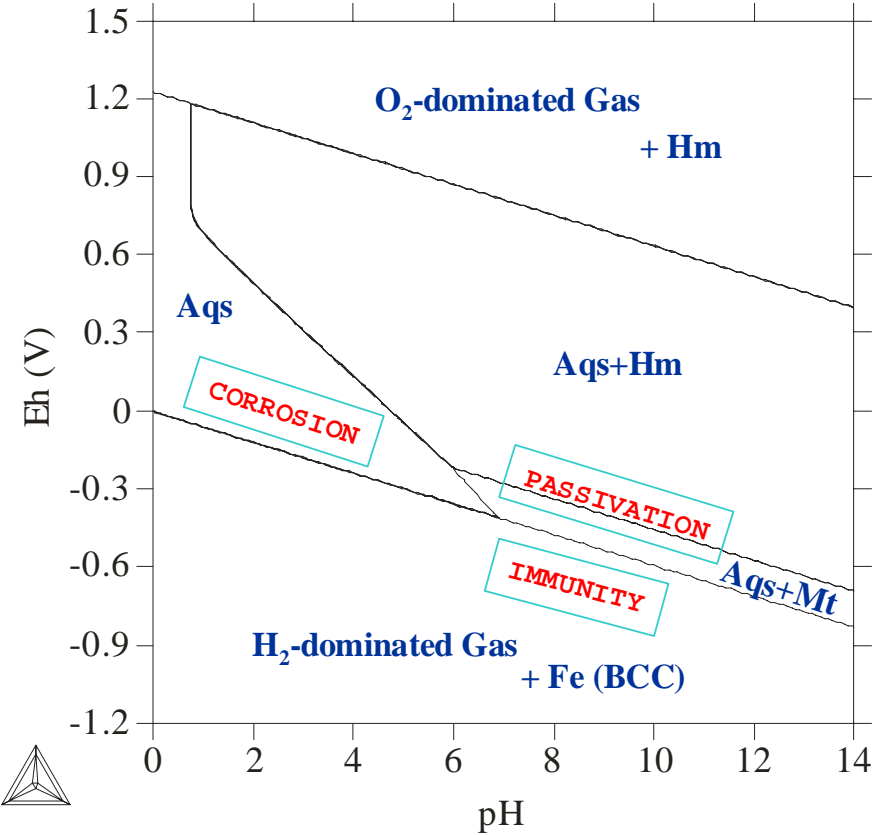


# Complete Pourbaix Diagrams !

1E-3m Fe in 1 kg of water at 25°C and 1 bar (Gas phase not included!)



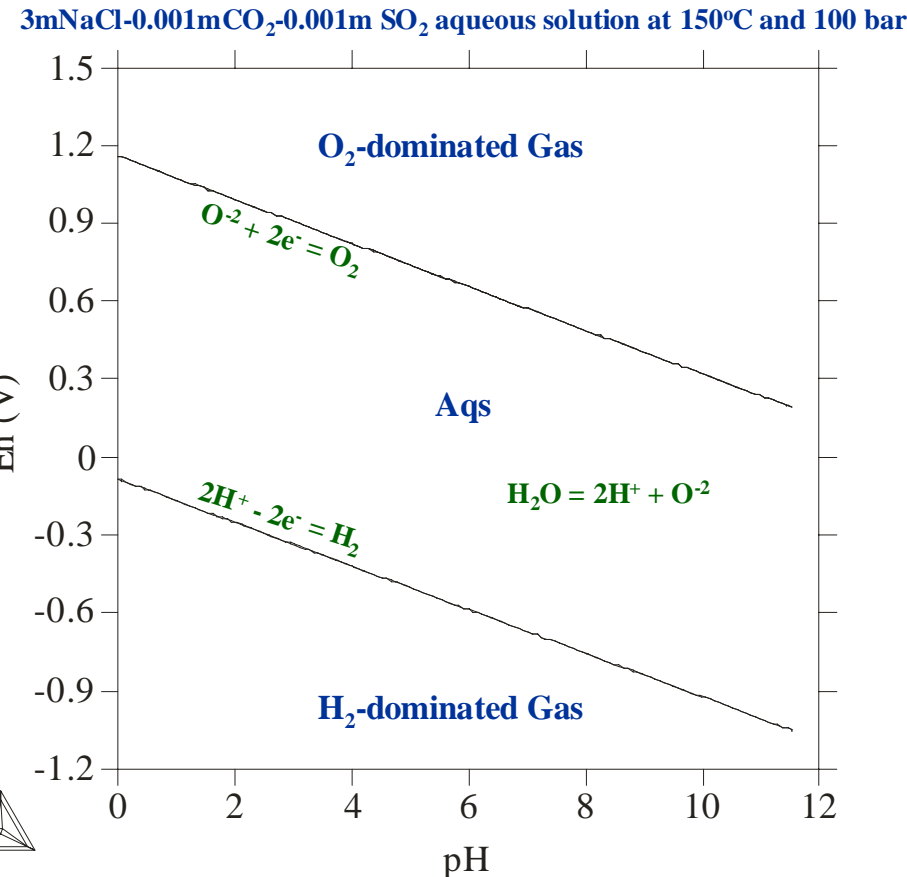
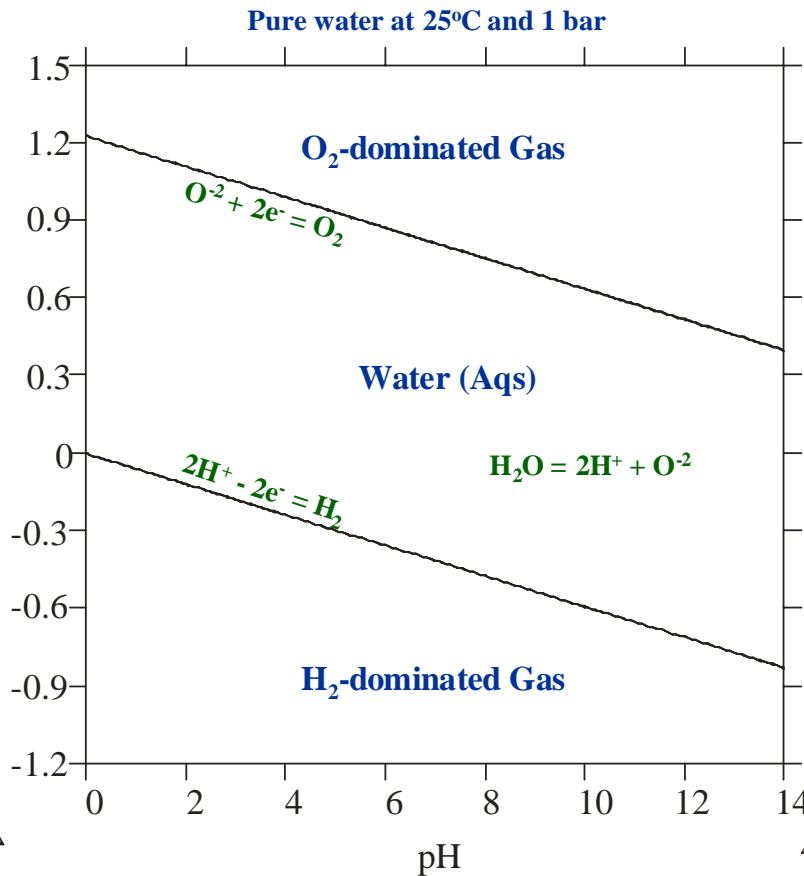
1E-3m Fe in 1 kg of water at 25°C and 1 bar (Gas phase included!)



“Pourbaix diagram” of Fe (with 0.001 mole Fe in 1 kg of pure water at 25°C and 1 bar; gas **excluded** in the calculation).

Pourbaix diagram of Fe (with 0.001 mole Fe in 1 kg of pure water at 25°C and 1 bar; gas **included** in the calculation).

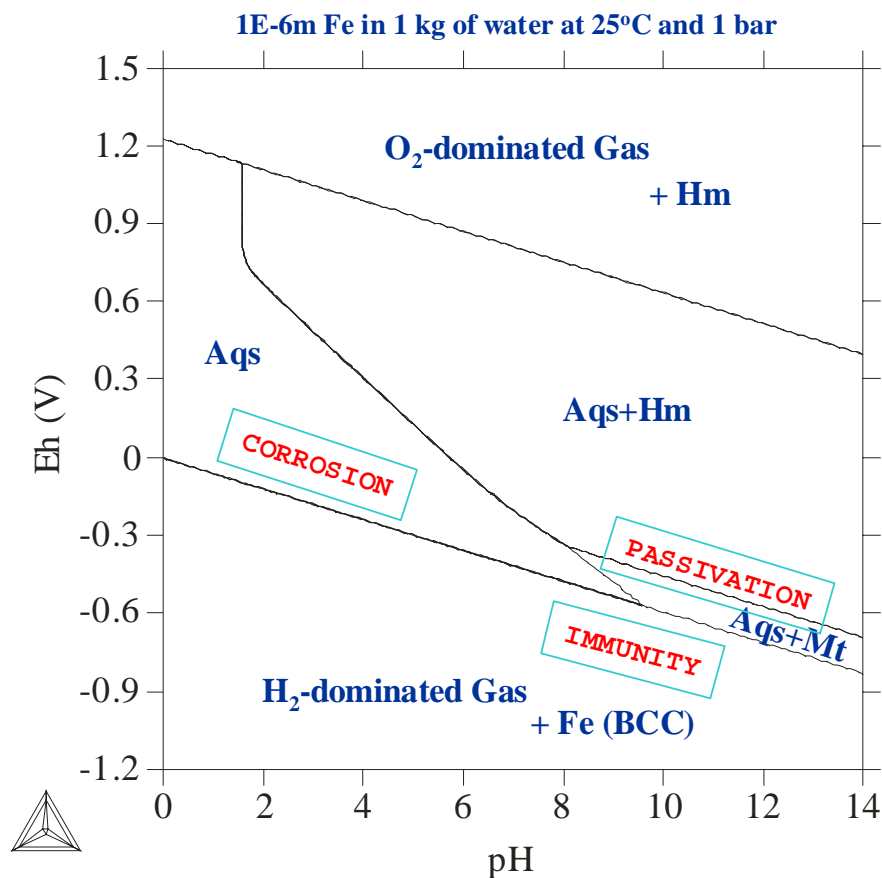
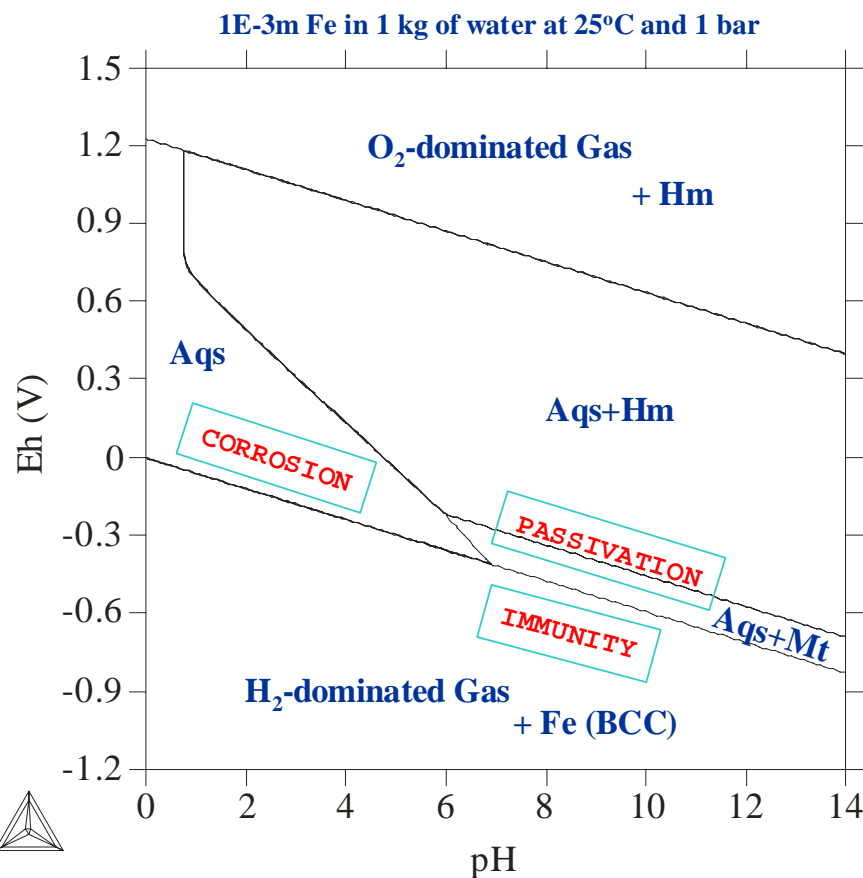
# Aqueous/Gaseous Phase Boundaries



The pH-Eh diagrams for pure water at 25°C and 1 bar, and for an 3mNaCl-0.001mCO<sub>2</sub>-0.001mSO<sub>2</sub> aqueous solution at 150°C and 100 bar.

# Pourbaix Diagrams: Simple Systems (I)

## Pure Fe: under various initial compositions

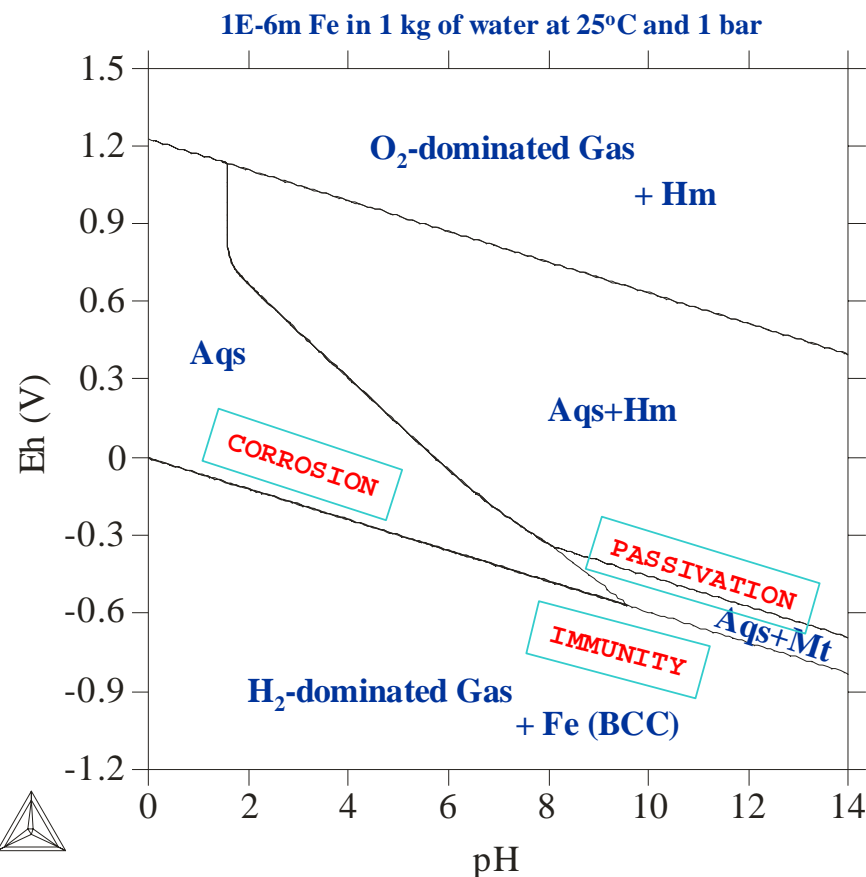


Pourbaix diagram of Fe (with **1E-3 mole Fe** in 1 kg of pure water) at 25°C and 1 bar.

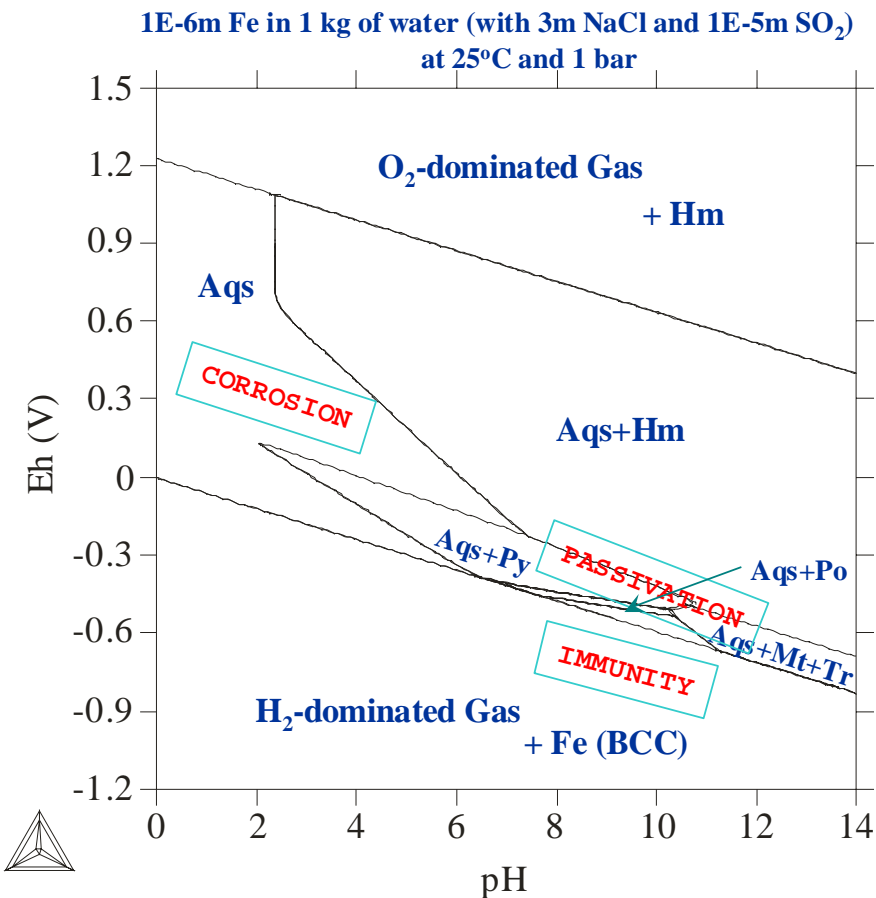
Pourbaix diagram of Fe (with **1E-6 mole Fe** in 1 kg of pure water) at 25°C and 1 bar.

# Pourbaix Diagrams: Simple Systems (II)

## Pure Fe: in different aqueous solutions



Pourbaix diagram of Fe (with 1E-6 mole Fe in 1 kg of pure water) at 25°C and 1 bar.

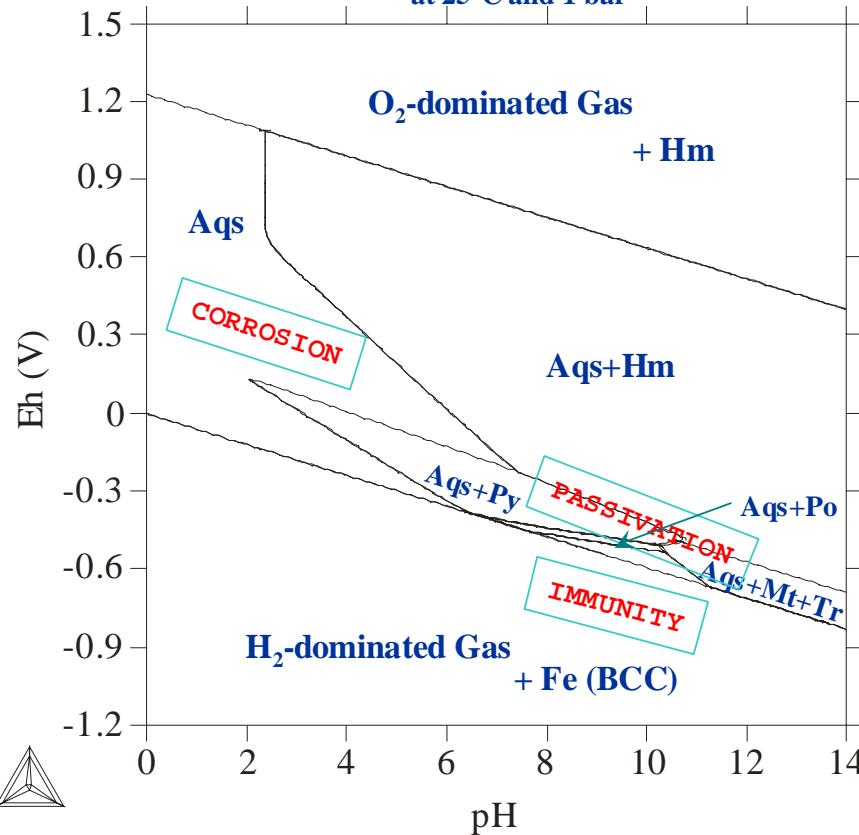


Pourbaix diagram of Fe (with 1E-6 mole Fe in 1 kg of water, 3m NaCl and 1E-5 m SO<sub>2</sub>) at 25°C and 1 bar.

# Pourbaix Diagrams: Simple Systems (III)

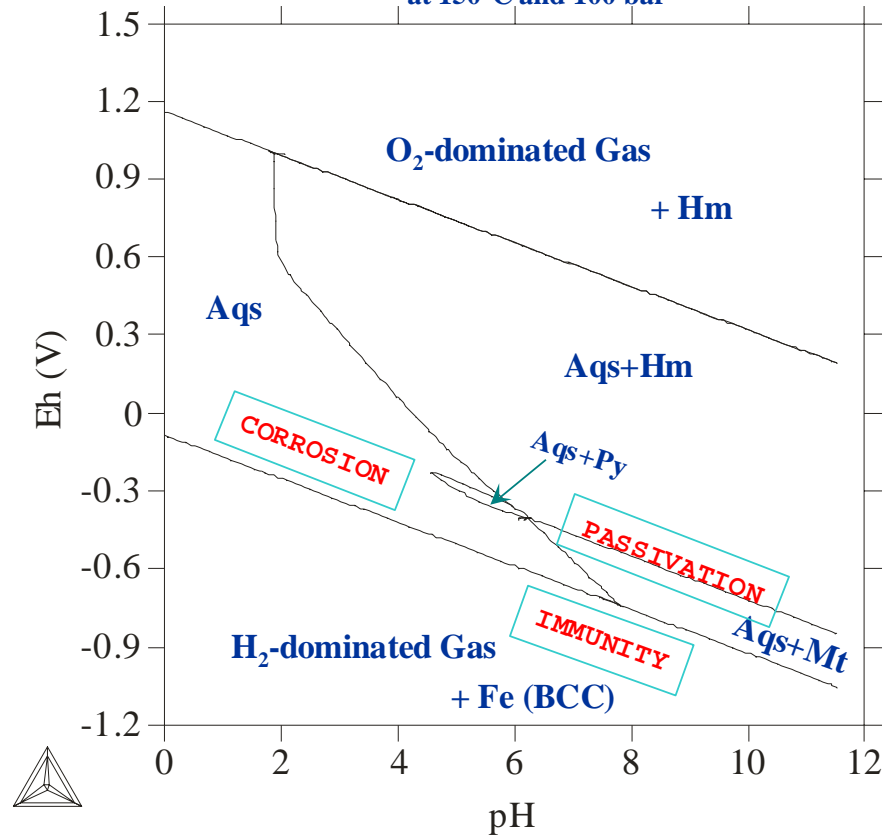
## Pure Fe: under different T-P conditions

1E-6m Fe in 1 kg of water (with 3m NaCl and 1E-5m SO<sub>2</sub>)  
at 25°C and 1 bar



Pourbaix diagram of Fe (with 1E-6 mole Fe in 1 kg of water, 3m NaCl and 1E-5 m SO<sub>2</sub>) at 25°C and 1 bar.

1E-6m Fe in 1 kg of water (with 3m NaCl and 1E-5m SO<sub>2</sub>)  
at 150°C and 100 bar



Pourbaix diagram of Fe (with 1E-6 mole Fe in 1 kg of water, 3m NaCl and 1E-5 m SO<sub>2</sub>) at 150°C and 100 bar.

The shape of a Pourbaix diagram of a complex multi-component alloy and the stability relations of various secondary phases (oxides, hydroxides, sulfides, sulfates, carbonates, nitrates, silicates, halides, or other forms) depend upon the following factors:

- *Initial amount and composition of the alloy/solid materials;*
- *Initial amount and composition of the interacting aqueous solution phase;*
- *Temperature and pressure conditions;*
- *Model treatments on various primary phases and secondary phases: solution or compound*

# Complete Pourbaix Diagrams via TC

Thermo-Calc can calculate Pourbaix diagrams and property diagrams, for various multi-component systems with:

- *Complex solution and compound phases (steels/Fe-based alloys, Ni-/Co-based superalloys, Al-/Mg-/Cu-/Ti-/Zr-based alloys, solder alloys, hard materials, ceramics, fuel-cell materials, oxides/hydroxides/sulfides/sulphates/silicates/carbonates/..., etc.), treated by various thermodynamic models;*
- *Complex aqueous solutions, treated by SIT, HKF & Pitzer models;*
- *Complex gaseous mixtures, treated by ideal & non-ideal EOS and mixing models;*
- *Wide temperature and pressure ranges.*

# Pourbaix Diagrams: Advantages from TC

- |                         |   |
|-------------------------|---|
| Complex Phases:         | Alloy compound/solution phases;<br>Oxide/Sulfide/Silicate/... solution phases;<br>Aqueous solution phases;<br>Gaseous mixture phases. |
| Complex Environments:   | Very wide P-T ranges;<br>Concentrated aqueous solutions.  |
| Multiple Functionality: | Many types of phase diagrams &<br>property diagrams   |

# Pourbaix Diagrams: TC vs Others

Specifications	Thermo-Calc	FACTSage, HSC
<i>Primary phases</i>	Complex alloy solutions (e.g. BCC, FCC, HCP; Sigma, Cementite)	Pure metals (e.g. Fe, Cr)
<i>Secondary phases</i>	Complex ( <i>solution</i> ) oxides/sulfides/silicates/...	Simple ( <i>stoichiometric</i> ) oxides/sulfides/silicates/...
<i>Gaseous mixtures</i>	Ideal/Non-ideal gas mixtures	Ideal gases
<i>Aqueous solutions</i>	Concentrated solutions	Dilute solutions
<i>Applicable P-T</i>	Wide P-T range (up to 5 kbar & 1000°C)	Room P-T conditions
<i>Calculation Tech</i>	Global Minimization + POLY GEM	Normal GEM or EC
<i>Predominance Area</i>	No	Y/N
<i>Property Plots</i>	Yes	No
<i>User's Database</i>	Yes	Y/N
<i>Data Assessments</i>	Yes	No
API	<i>To be implemented</i> (TQ/TCAPI)	No

The following types of calculations can be performed by using the Thermo-Calc software and selective databases, for investigations of corrosion processes of various steels/alloys.

- *Mapping Calculations of Eh-pH diagrams (i.e., the so-called Pourbaix diagrams), and various property diagrams which are relevant to different phase boundaries on a corresponding Eh-pH diagrams;*
- *Mapping or Stepping Calculations of heterogeneous interactions, by changing one or two (or more) controlling variables (temperature, pressure, acidity, electronic potential, salinity, aqueous concentration, alloy composition, etc.)*

A lot of interesting diagrams can be easily calculated and graphically generated, which can be conveniently edited, refined, printed and saved.

# Case 1: Corrosion of Stainless Steel

**Initial composition of a specific stainless steel (austenite):**

<i>Element</i>	<i>Composition (wt%)</i>	<i>Composition (X)</i>
Fe	68.50	0.687523
Cr	17.00	0.183263
Ni	12.00	0.114608
Mo	2.50	0.014606

**Initial composition of interacting aqueous solution:**

**H<sub>2</sub>SO<sub>4</sub> 5% (0.537 molality)**

**Initial temperature and pressure of exposure:**

**85°C and 1 bar**

# Case 1: Corrosion of Stainless Steel

## Data Resources:

<b>TCFE5</b>	<b>TCS Steels/Fe-Alloys (Solutions) Database</b> <b>Steel/Alloy Phases, Oxide/Sulfide Solutions</b>
<b>ION2</b>	<b>TCS Oxides/Sulfides (Solutions) Database</b> <b>Oxide/Sulfide/Silicate Solutions</b>
<b>SSUB4</b>	<b>SGTE Substances (Compounds) Database</b> <b>Gaseous mixture,</b> <b>Oxides, Hydroxides, Sulfides, Sulphates,</b> <b>Halides, complex salts</b>
<b>TCAQ2</b>	<b>TCS Aqueous Solution Database</b> <b>Aqueous solution (using SIT model)</b>
<b>AQS2</b>	<b>TGG Aqueous Solution Database</b> <b>Aqueous solution (using HKF model)</b>

- Calculations:**
- 1: Pourbaix diagram and property diagrams  
*Mapping in pH and Eh*
  - 2: Property diagrams  
*Stepping in Eh*
  - 3: Property diagrams  
*Stepping in temperature*

## Calculation 1: Pourbaix Diagram Calculation

### Bulk composition:

0.1 g stainless steel (i.e., 0.001784 mole austenite)

1 kg H<sub>2</sub>O, with [SO<sub>4</sub><sup>-2</sup>]=0.537 molality

### T-P conditions:

85°C and 1 bar

### Mapping variables:

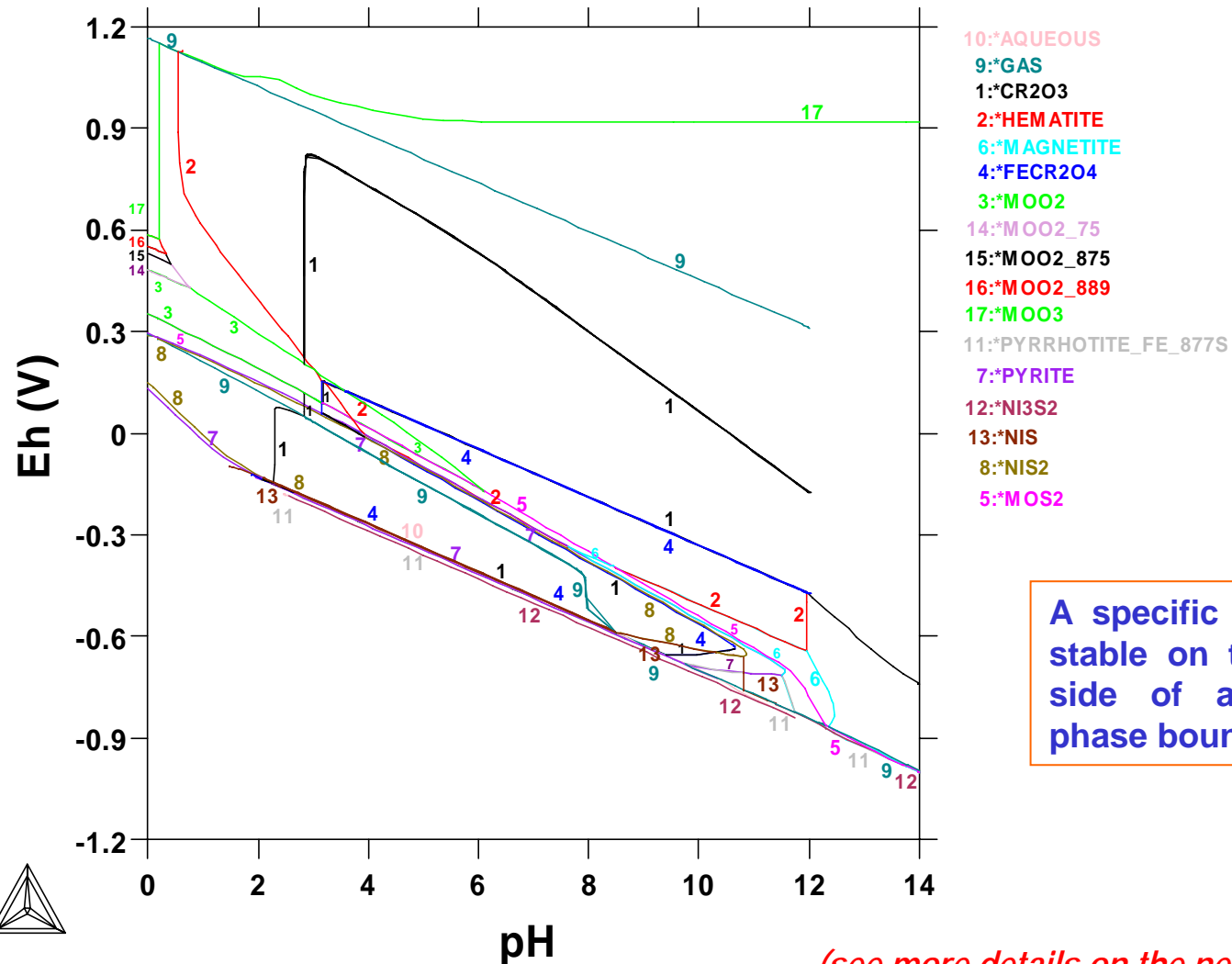
pH and Eh

# Case 1: Corrosion of Stainless Steel

## Calculation 1: Pourbaix Diagram

$T=358.15\text{ K}$ ,  $P=1\text{ bar}$ ,  $B(\text{H}_2\text{O})=1000\text{ g}$ ,  $N(\text{H}_2\text{SO}_4)=0.537\text{ m}$

$N(\text{Fe})=1.2266\text{E-}3$ ,  $N(\text{Cr})=3.2695\text{E-}4$ ,  $N(\text{Mo})=2.6058\text{E-}5$ ,  $N(\text{Ni})=2.0446\text{E-}4$

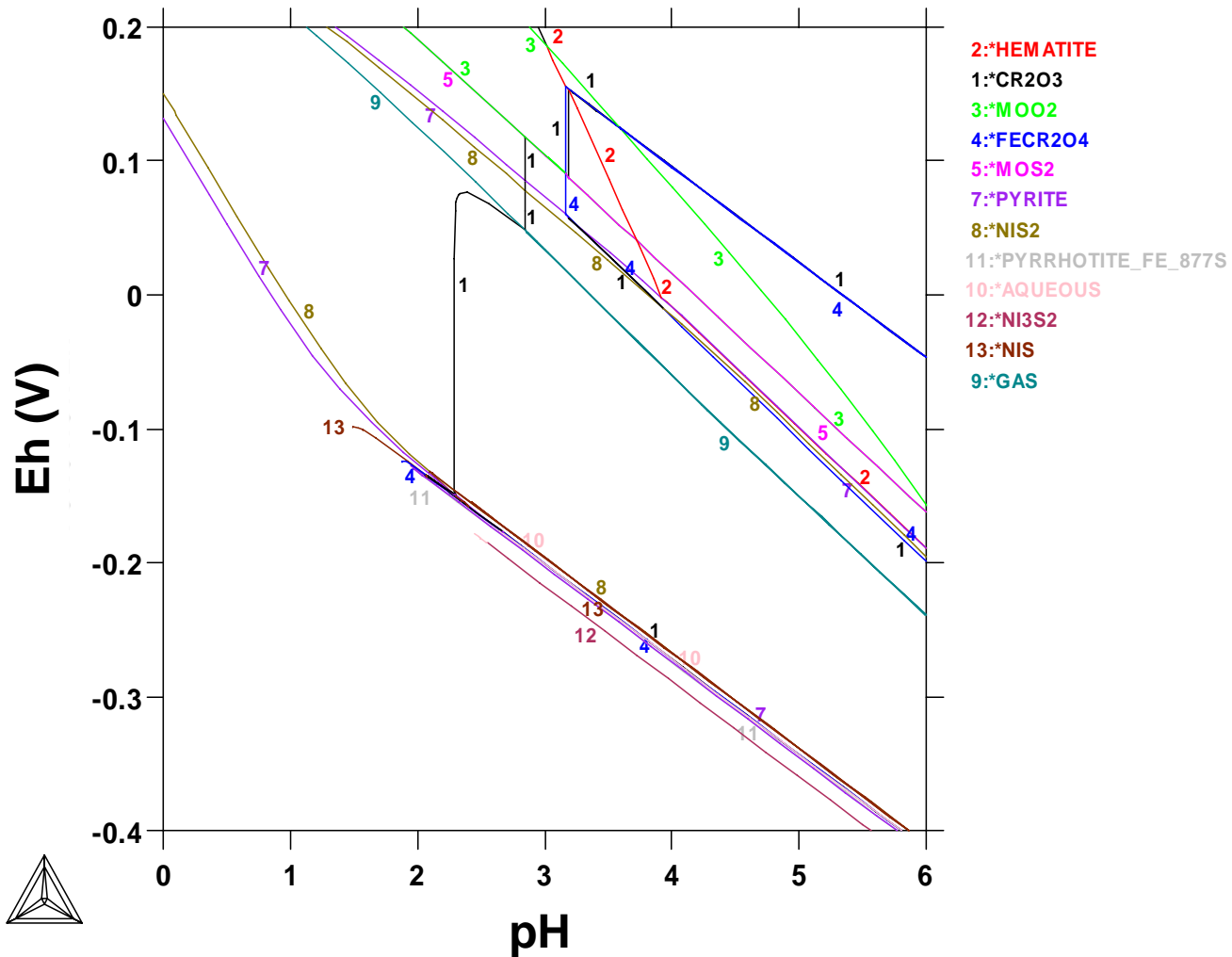


(see more details on the next two slides)

# Case 1: Corrosion of Stainless Steel

## Calculation 1: Pourbaix Diagram (enlarged for the low pH range)

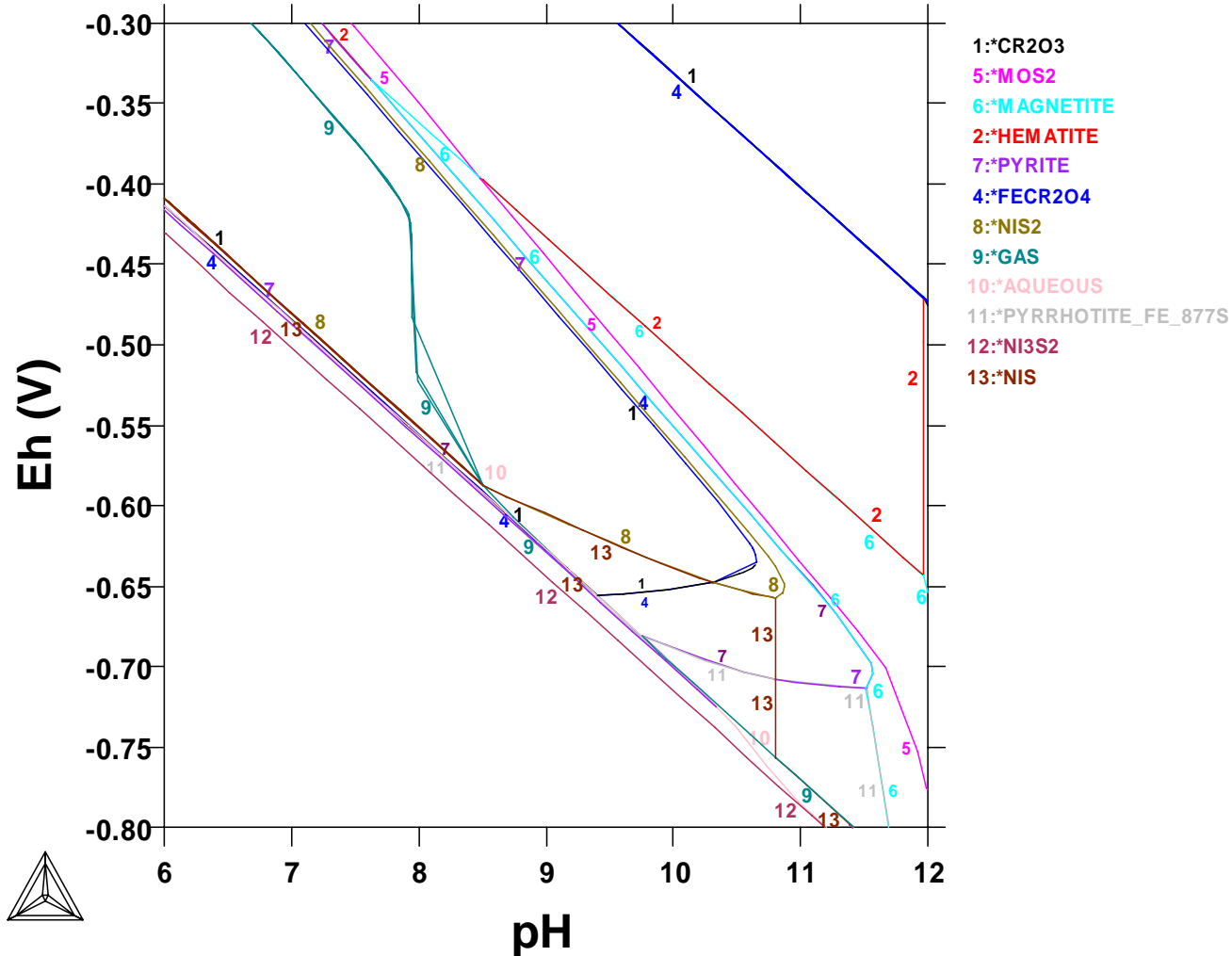
$T=358.15$  K,  $P=1$  bar,  $B(\text{H}_2\text{O})=1000$  g,  $N(\text{H}_2\text{SO}_4)=0.537$  m  
 $N(\text{Fe})=1.2266\text{E-}3$ ,  $N(\text{Cr})=3.2695\text{E-}4$ ,  $N(\text{Mo})=2.6058\text{E-}5$ ,  $N(\text{Ni})=2.0446\text{E-}4$



# Case 1: Corrosion of Stainless Steel

## Calculation 1: Pourbaix Diagram (enlarged for the high pH range)

$T=358.15\text{ K}$ ,  $P=1\text{ bar}$ ,  $B(\text{H}_2\text{O})=1000\text{ g}$ ,  $N(\text{H}_2\text{SO}_4)=0.537\text{ m}$   
 $N(\text{Fe})=1.2266\text{E-}3$ ,  $N(\text{Cr})=3.2695\text{E-}4$ ,  $N(\text{Mo})=2.6058\text{E-}5$ ,  $N(\text{Ni})=2.0446\text{E-}4$



## Calculation 2: Property Diagram Calculation

### Bulk composition:

0.1 g stainless steel (i.e., 0.001784 mole austenite)

1 kg H<sub>2</sub>O, with [H<sub>2</sub>SO<sub>4</sub>]=0.537 molality (i.e., 5wt%)

### T-P conditions:

85°C and 1 bar

### Stepping variable:

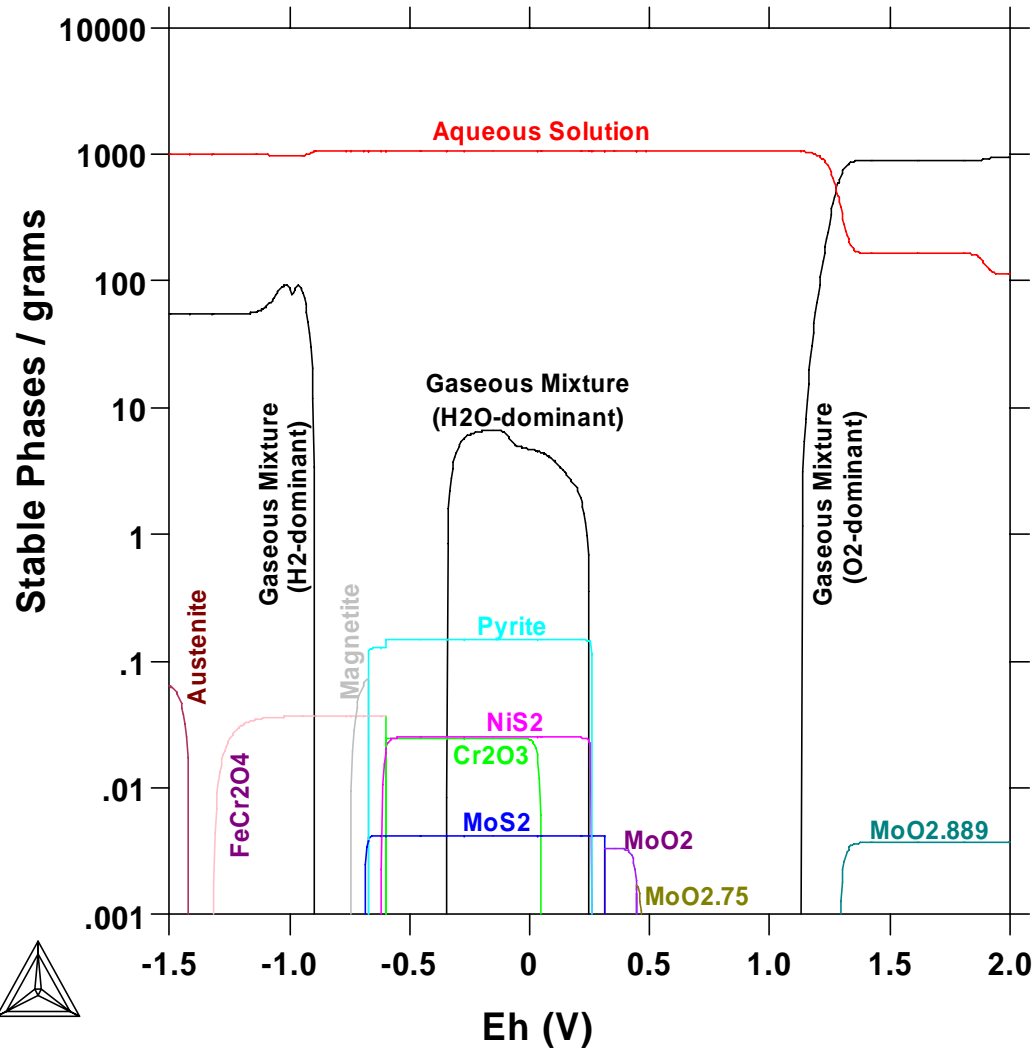
Eh (from -1.5 to 2.0 V)

# Case 1: Corrosion of Stainless Steel

## Calculation 2: Stable Phase Compositions varied with Eh condition

$T=358.15\text{ K}$ ,  $P=1\text{ bar}$ ,  $B(\text{H}_2\text{O})=1000\text{ g}$ ,  $N(\text{H}_2\text{SO}_4)=0.537\text{ m}$

$N(\text{Fe})=1.2266\text{E-}3$ ,  $N(\text{Cr})=3.2695\text{E-}4$ ,  $N(\text{Mo})=2.6058\text{E-}5$ ,  $N(\text{Ni})=2.0446\text{E-}4$



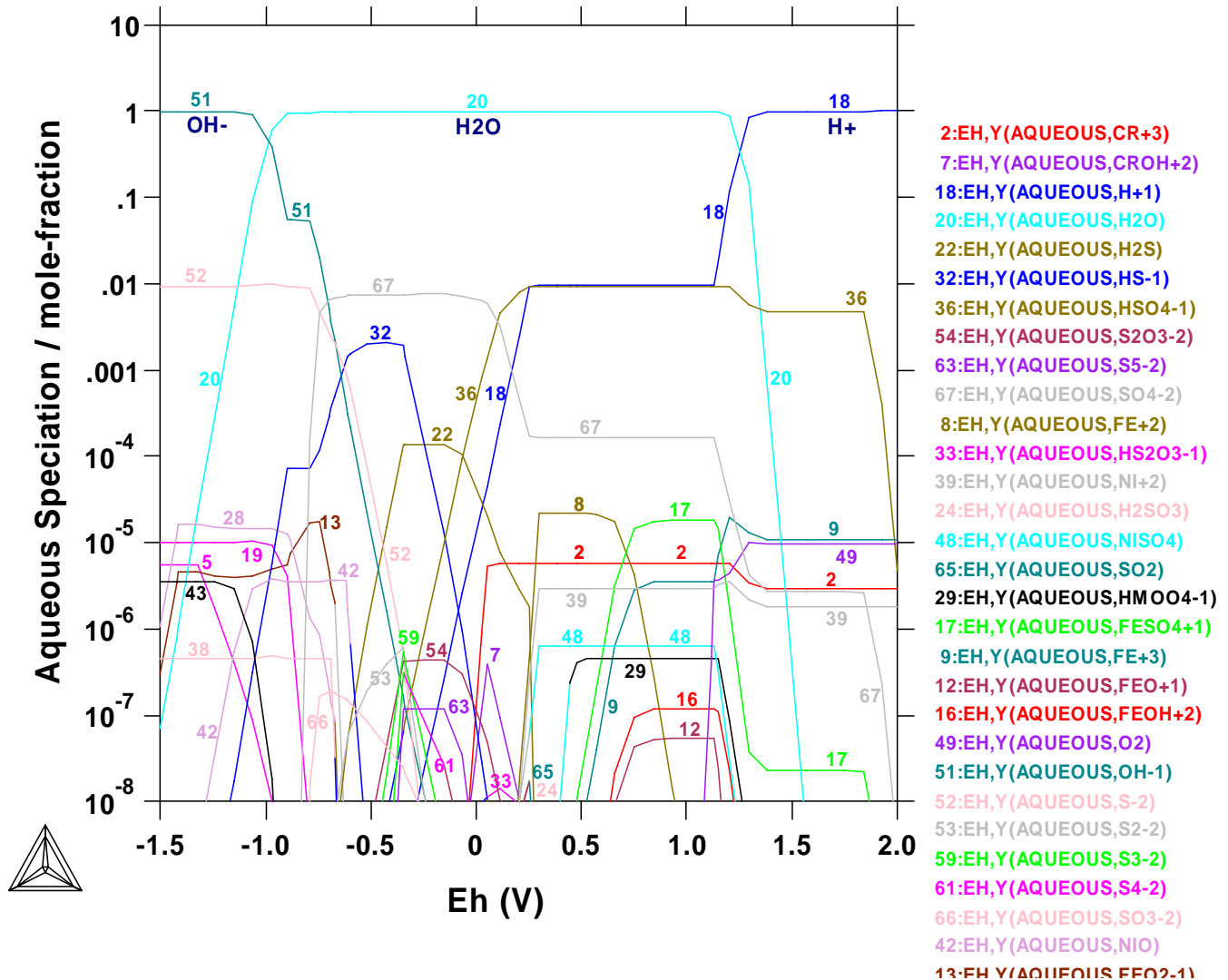
Complex oxide and sulfide solution phases have all been suspended from this testing calculation.

# Case 1: Corrosion of Stainless Steel

## Calculation 2: Major Aqueous Speciation varied with Eh condition:

$T=358.15\text{ K}$ ,  $P=1\text{ bar}$ ,  $B(\text{H}_2\text{O})=1000\text{ g}$ ,  $N(\text{H}_2\text{SO}_4)=0.537\text{ m}$

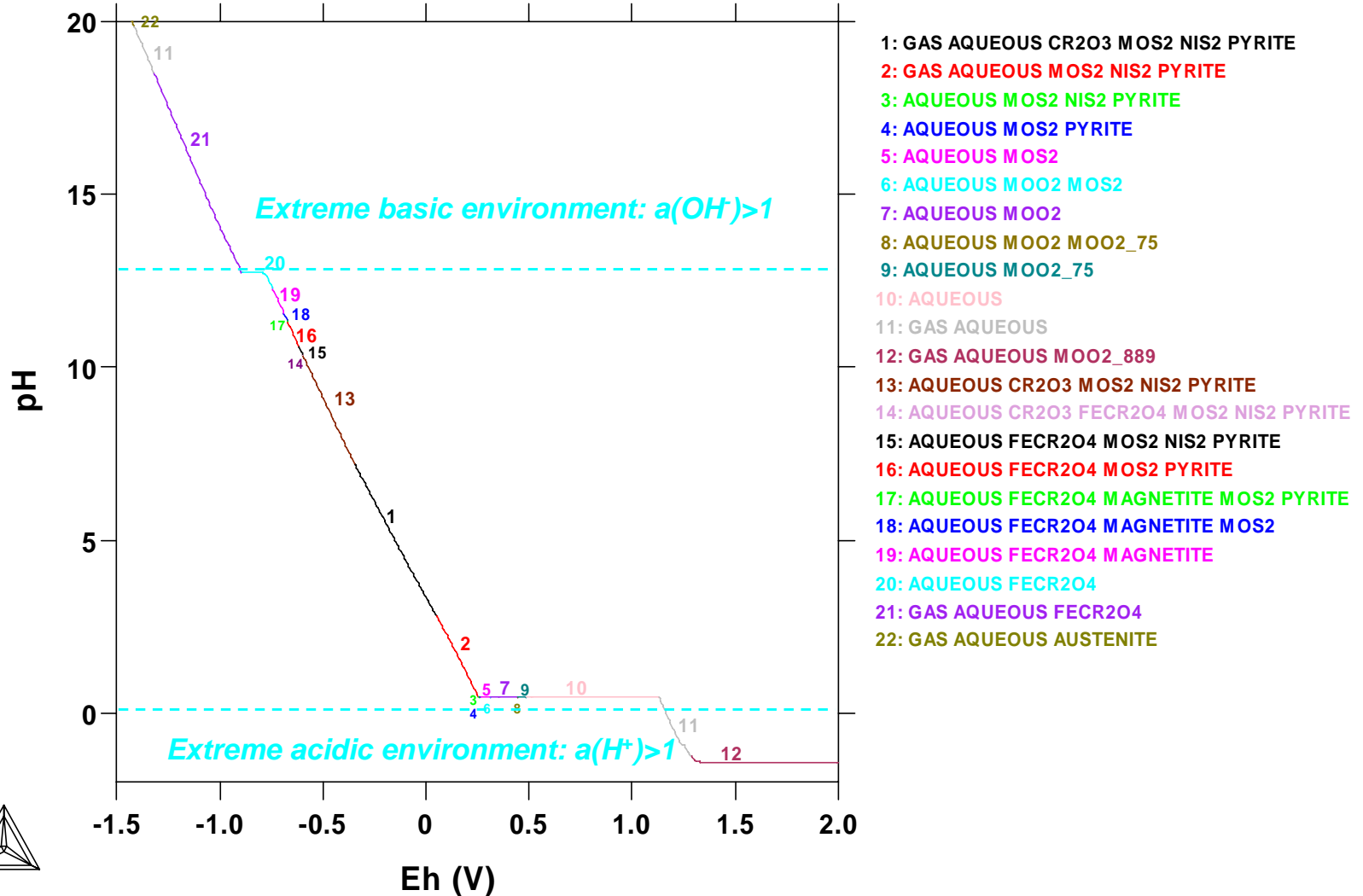
$N(\text{Fe})=1.2266\text{E-}3$ ,  $N(\text{Cr})=3.2695\text{E-}4$ ,  $N(\text{Mo})=2.6058\text{E-}5$ ,  $N(\text{Ni})=2.0446\text{E-}4$



# Case 1: Corrosion of Stainless Steel

## Calculation 2: Ph value varied with Eh condition

$T=358.15$  K,  $P=1$  bar,  $B(\text{H}_2\text{O})=1000$  g,  $N(\text{H}_2\text{SO}_4)=0.537$  m  
 $N(\text{Fe})=1.2266\text{E-}3$ ,  $N(\text{Cr})=3.2695\text{E-}4$ ,  $N(\text{Mo})=2.6058\text{E-}5$ ,  $N(\text{Ni})=2.0446\text{E-}4$



## Calculation 3: Property Diagram Calculation

### Bulk composition:

0.1 g stainless steel (i.e., 0.001784 mole austenite)

1 kg H<sub>2</sub>O, with [H<sub>2</sub>SO<sub>4</sub>]=0.537 molality (i.e., 5wt%)

### P condition:

1 bar

### Eh condition:

Electronically balanced (Eh=0)

### Stepping variable:

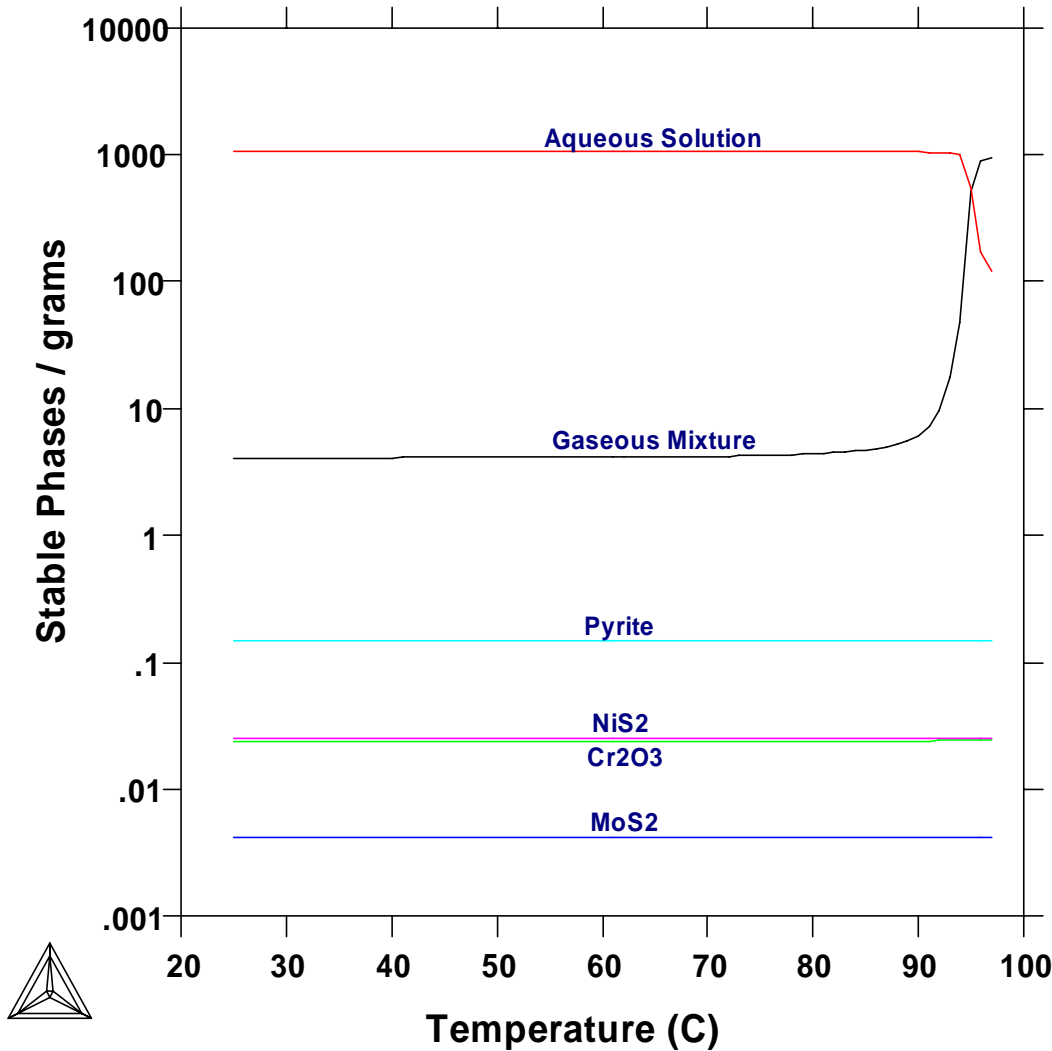
Temperature (from 25°C to boiling temperature)

# Case 1: Corrosion of Stainless Steel

## Calculation 3: Stable Phase Compositions varied with temperature condition

$P=1$  bar,  $B(\text{H}_2\text{O})=1000$  g,  $N(\text{H}_2\text{SO}_4)=0.537$  m

$N(\text{Fe})=1.2266\text{E-}3$ ,  $N(\text{Cr})=3.2695\text{E-}4$ ,  $N(\text{Mo})=2.6058\text{E-}5$ ,  $N(\text{Ni})=2.0446\text{E-}4$



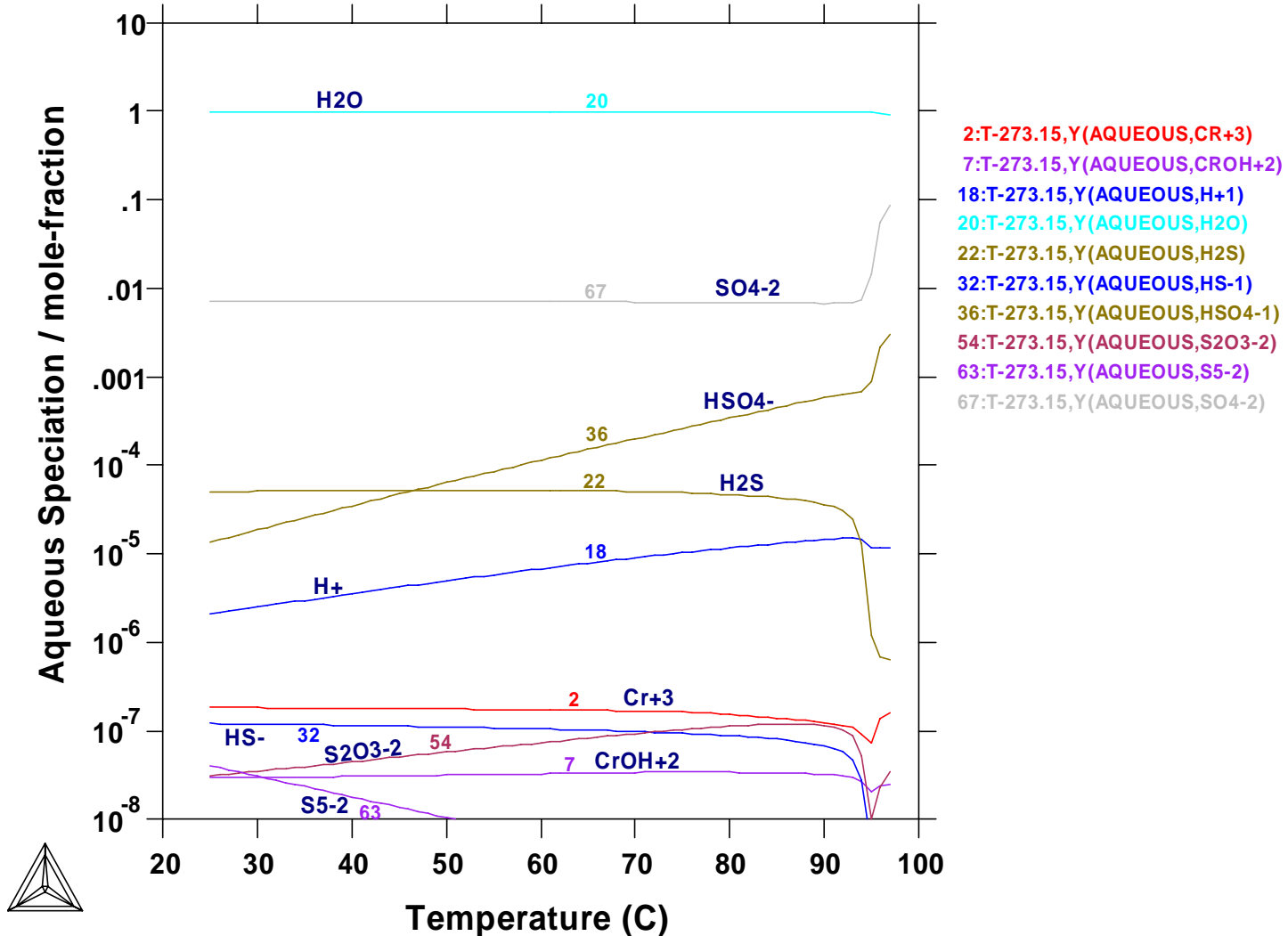
Complex oxide and sulfide solution phases have all been suspended from this testing calculation.

# Case 1: Corrosion of Stainless Steel

## Calculation 3: Aqueous Speciation varied with temperature condition: Part 1

$P=1$  bar,  $B(\text{H}_2\text{O})=1000$  g,  $N(\text{H}_2\text{SO}_4)=0.537$  m

$N(\text{Fe})=1.2266\text{E-}3$ ,  $N(\text{Cr})=3.2695\text{E-}4$ ,  $N(\text{Mo})=2.6058\text{E-}5$ ,  $N(\text{Ni})=2.0446\text{E-}4$

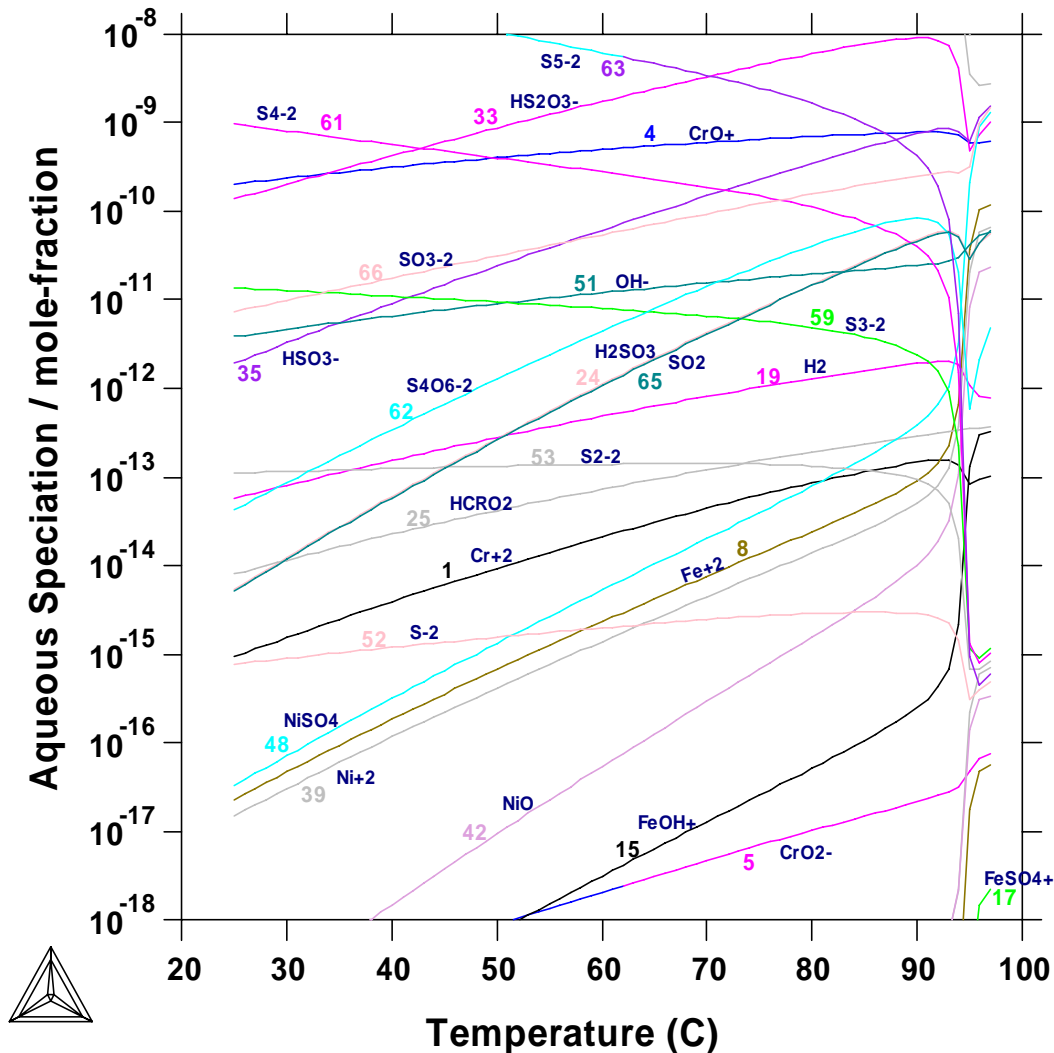


# Case 1: Corrosion of Stainless Steel

## Calculation 3: Aqueous Speciation varied with temperature condition: Part 2

$P=1$  bar,  $B(\text{H}_2\text{O})=1000$  g,  $N(\text{H}_2\text{SO}_4)=0.537$  m

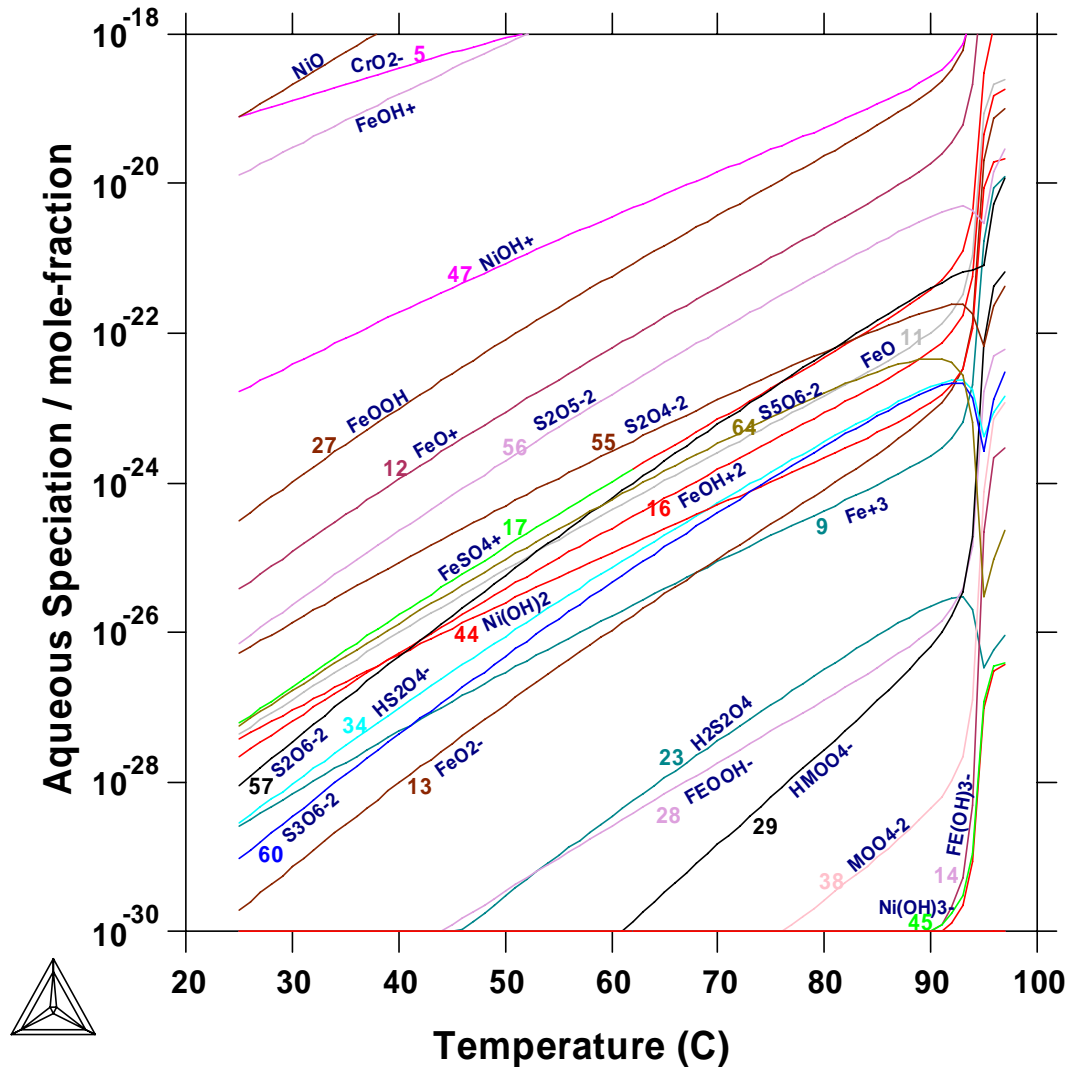
$N(\text{Fe})=1.2266\text{E-}3$ ,  $N(\text{Cr})=3.2695\text{E-}4$ ,  $N(\text{Mo})=2.6058\text{E-}5$ ,  $N(\text{Ni})=2.0446\text{E-}4$



# Case 1: Corrosion of Stainless Steel

## Calculation 3: Aqueous Speciation varied with temperature condition: Part 3

$P=1 \text{ bar}$ ,  $B(\text{H}_2\text{O})=1000 \text{ g}$ ,  $N(\text{H}_2\text{SO}_4)=0.537 \text{ m}$   
 $N(\text{Fe})=1.2266\text{E-}3$ ,  $N(\text{Cr})=3.2695\text{E-}4$ ,  $N(\text{Mo})=2.6058\text{E-}5$ ,  $N(\text{Ni})=2.0446\text{E-}4$

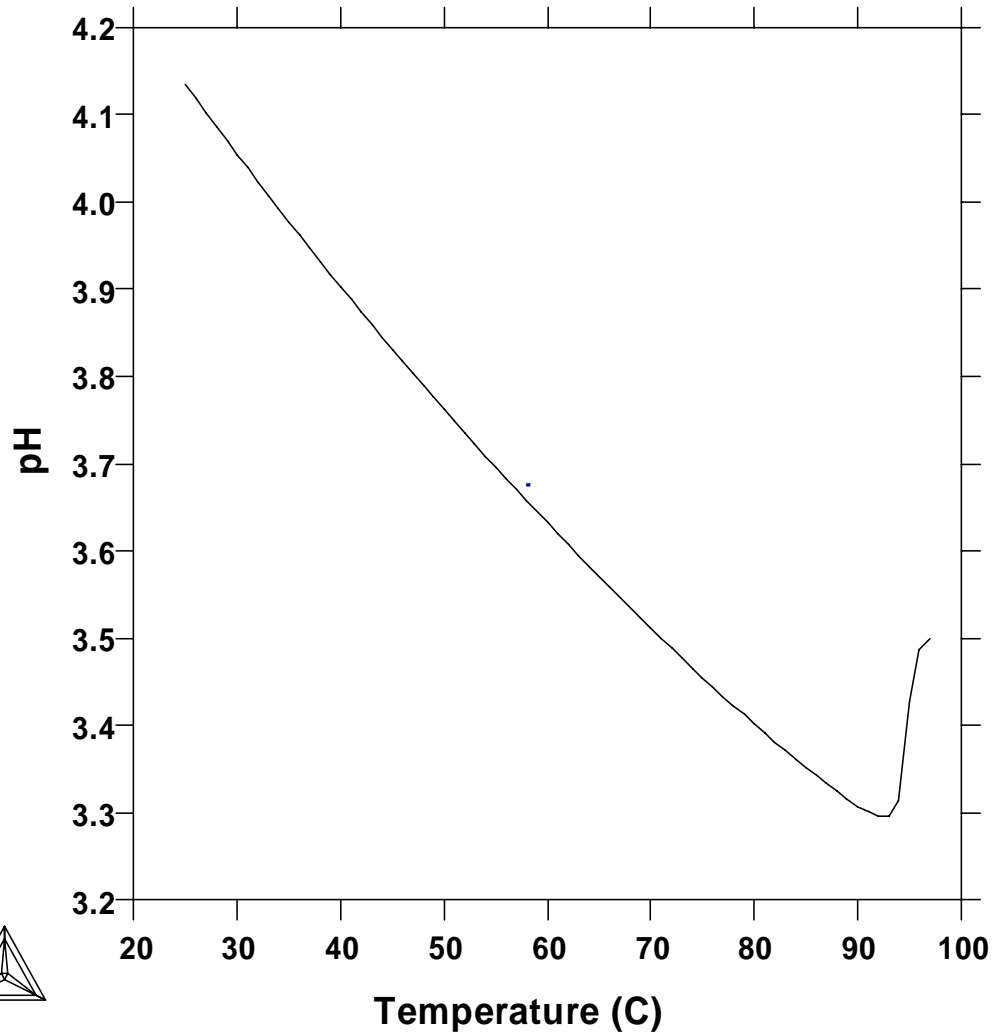


# Case 1: Corrosion of Stainless Steel

## Calculation 3: Ph value varied with temperature condition

$P=1$  bar,  $B(H_2O)=1000$  g,  $N(H_2SO_4)=0.537$  m

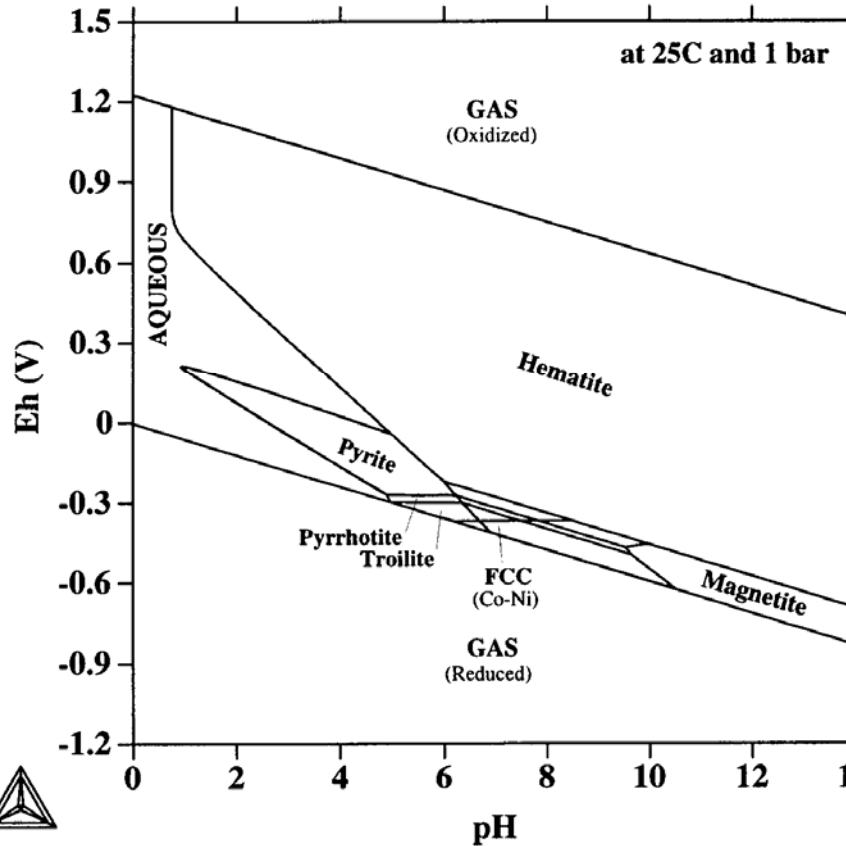
$N(Fe)=1.2266E-3$ ,  $N(Cr)=3.2695E-4$ ,  $N(Mo)=2.6058E-5$ ,  $N(Ni)=2.0446E-4$



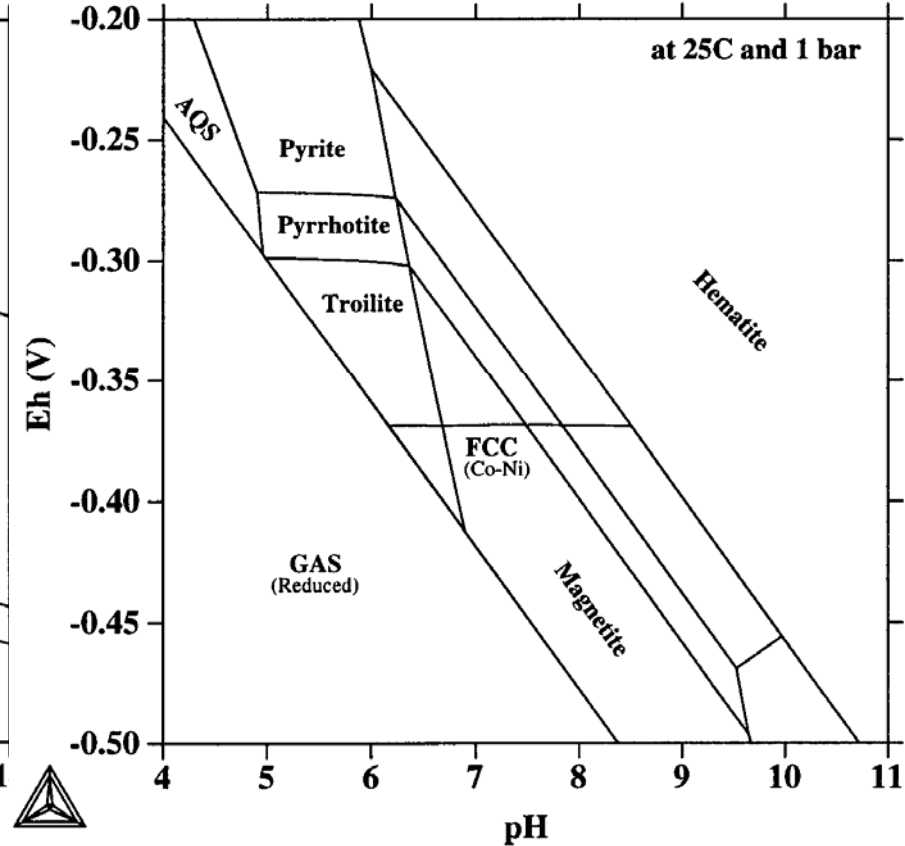


# Case 3: Corrosion of Steel

THERMO-CALC: POURBAIX Module Calculation  
1e-3mFe+5e-5mCo+5e-5mNi in 1 kg of water (with 1e-6mS)



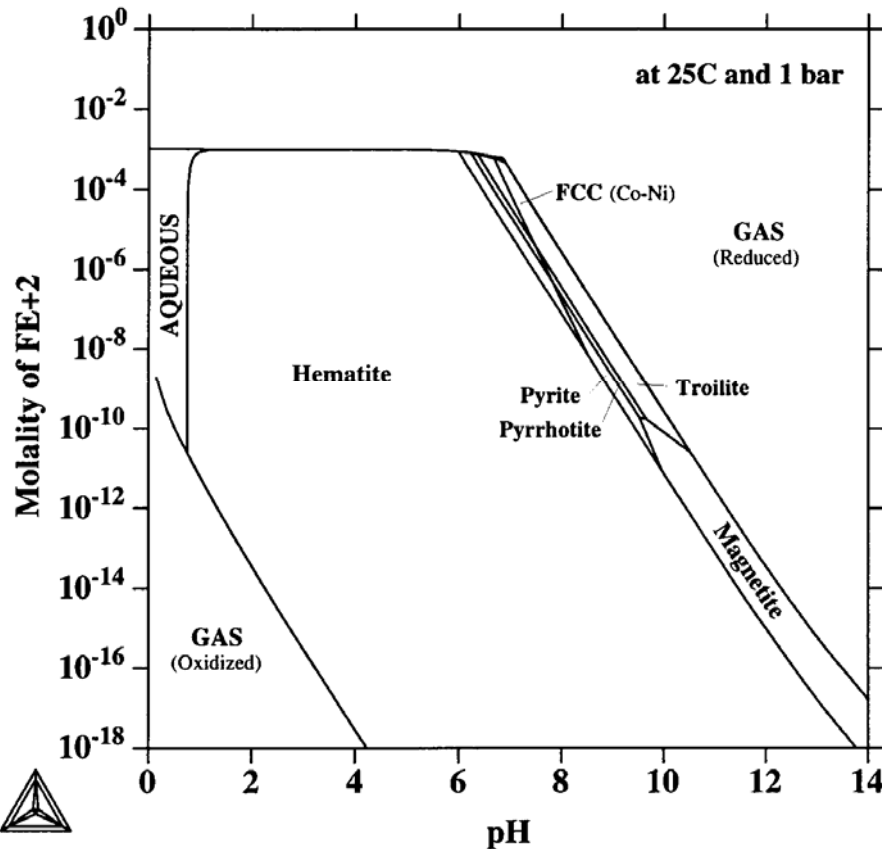
THERMO-CALC: POURBAIX Module Calculation  
1e-3mFe+5e-5mCo+5e-5mNi in 1 kg of water (with 1e-6mS)



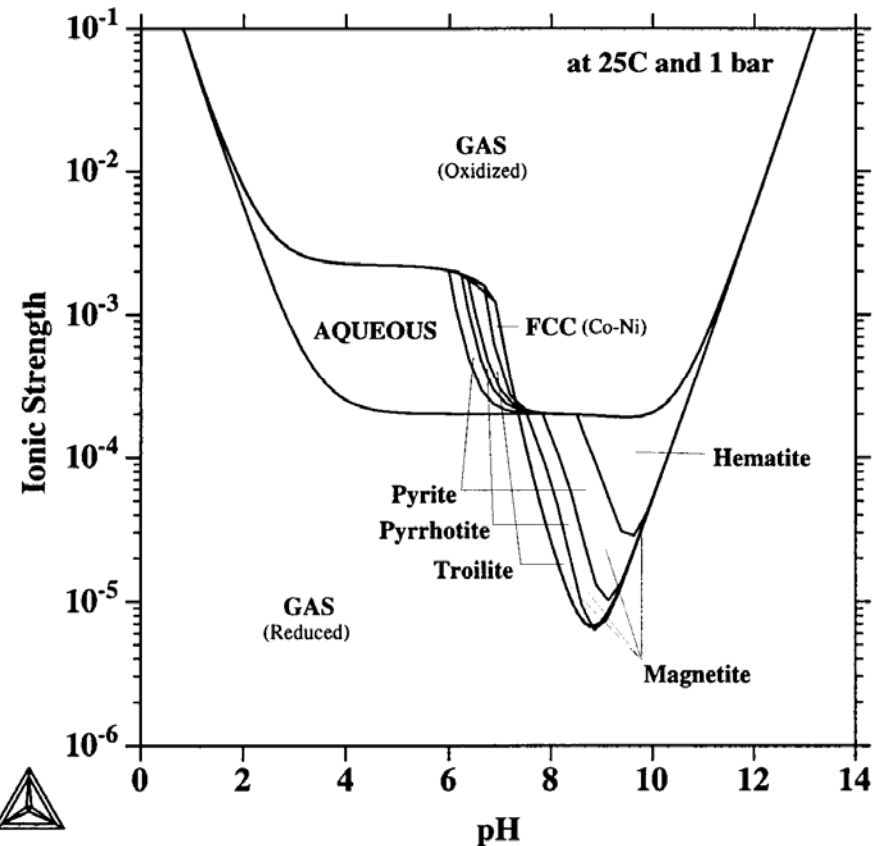
Pourbaix diagram and zoomed part of an Fe-Alloy (consisting of 1E-3 m Fe, 5E-5 m Co and 5E-5 m Ni), interacted with 1 kg of water (with 1E-6 m S) at 25°C and 1 bar.

# Case 3: Corrosion of Steel

THERMO-CALC: POURBAIX Module Calculation  
1e-3mFe+5e-5mCo+5e-5mNi in 1 kg of water (with 1e-6mS)

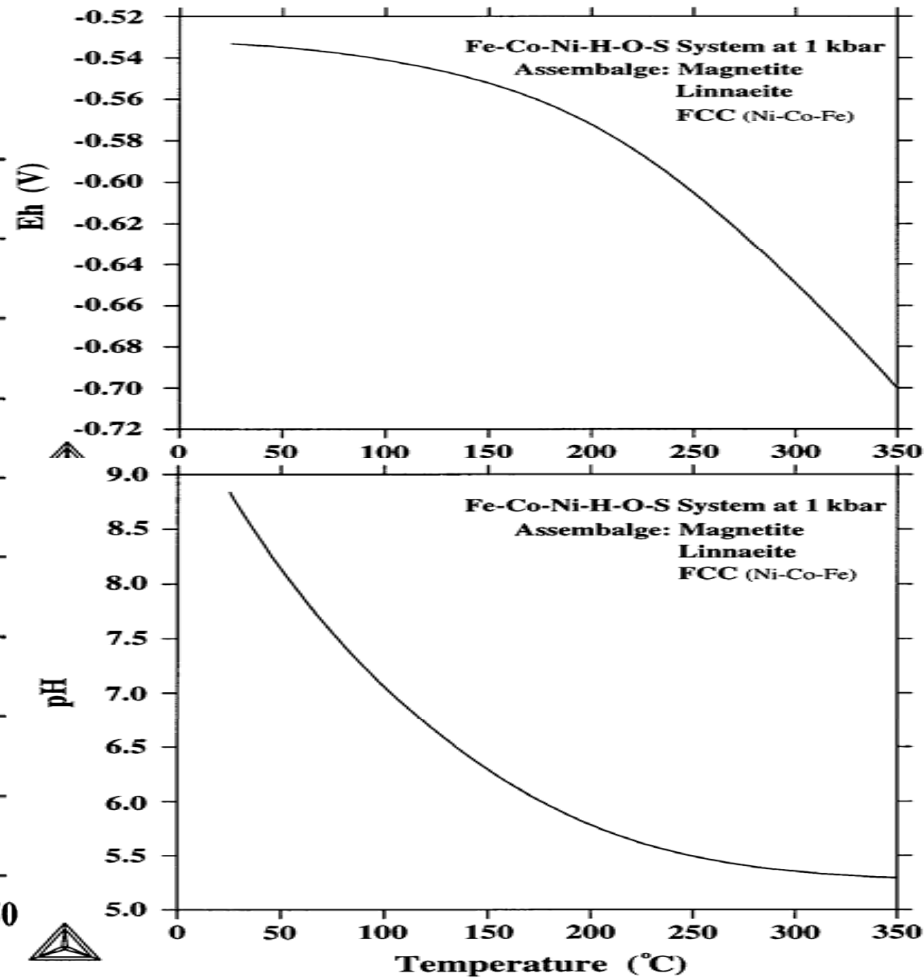
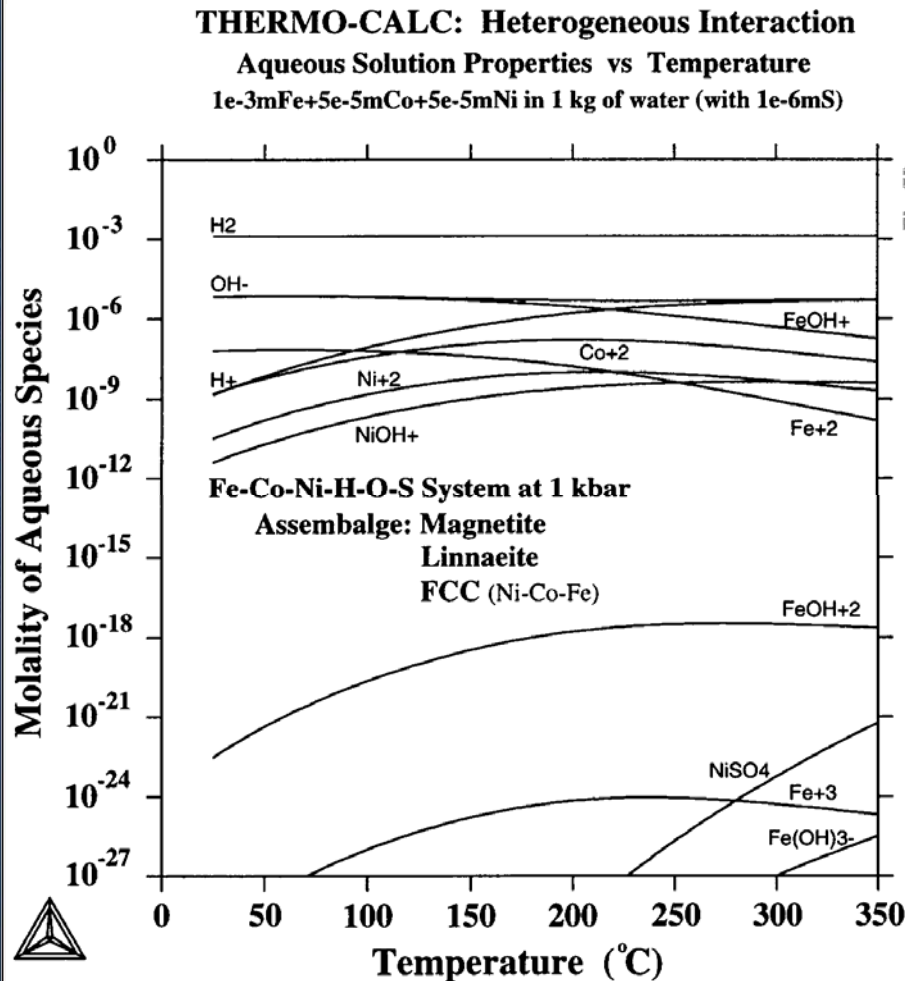


THERMO-CALC: POURBAIX Module Calculation  
1e-3mFe+5e-5mCo+5e-5mNi in 1 kg of water (with 1e-6mS)



$Fe^{+2}$  molality vs. pH and Ionic strength vs. pH diagrams for the heterogeneous interaction between an Fe-Alloy (consisting of 1E-3 m Fe, 5E-5 m Co and 5E-5 m Ni) and 1 kg of water (with 1E-6 m S) at 25°C and 1 bar.

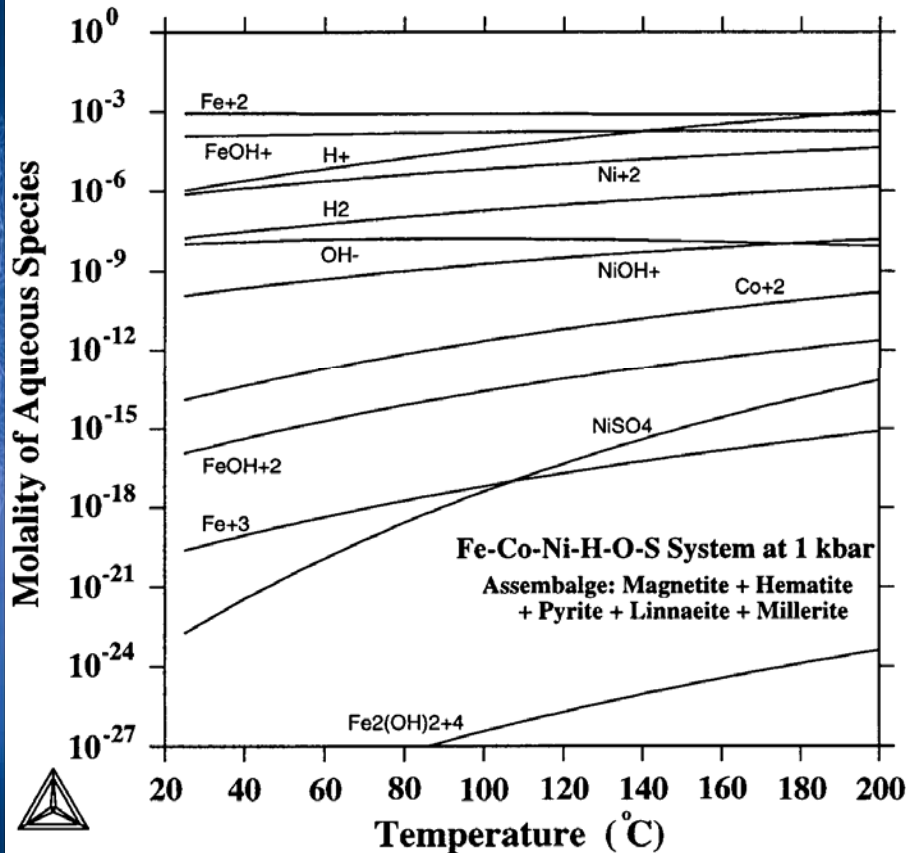
# Case 3: Corrosion of Steel



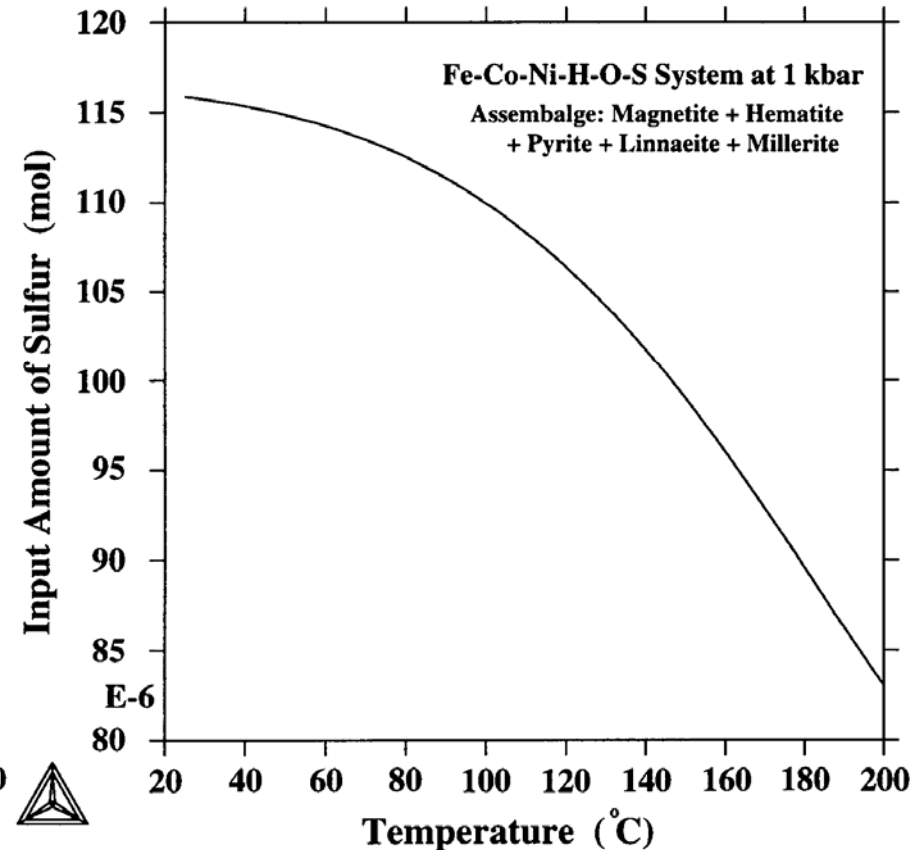
Dependencies of aqueous concentration, Eh and pH on temperature for the equilibrium assemblage Magnetite-Linnaeite-FCC(Ni-Co-Fe) in the heterogeneous interaction between an Fe-Alloy (consisting of 1E-3 m Fe, 5E-5 m Co and 5E-5 m Ni) and 1 kg of water (with 1E-6 m S) at 1 kbar.

# Case 3: Corrosion of Steel

**THERMO-CALC: Heterogeneous Interaction**  
Aqueous Solution Properties vs Temperature  
1e-3mFe+5e-5mCo+5e-5mNi in 1 kg of water (open to S)



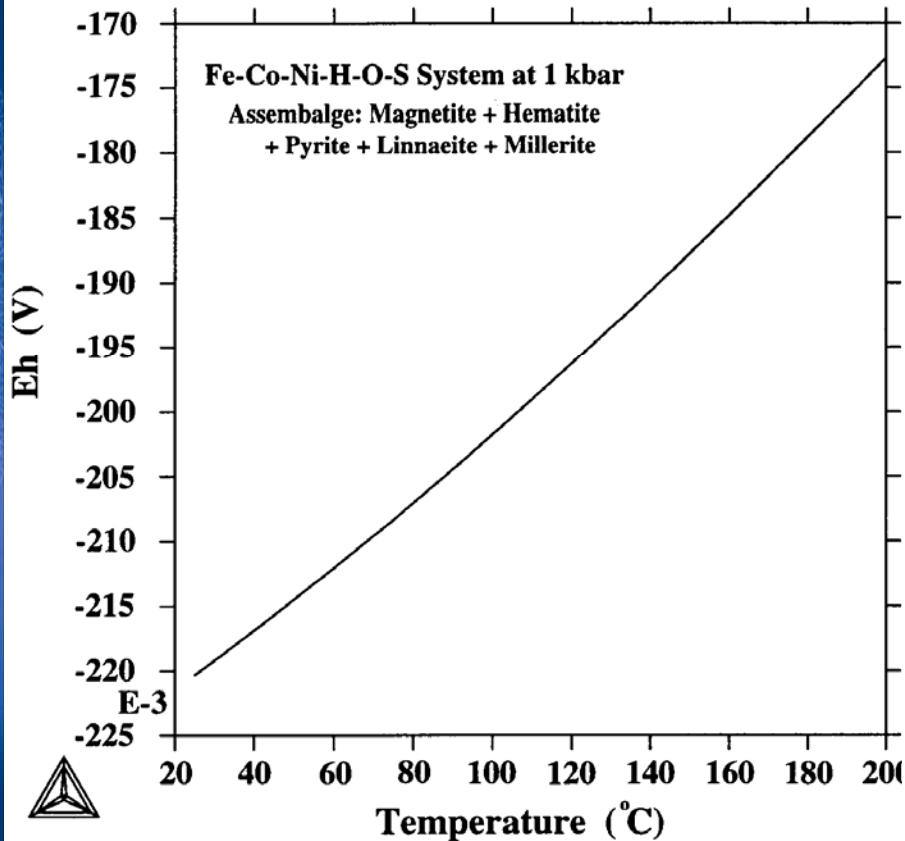
**THERMO-CALC: Heterogeneous Interaction**  
Aqueous Solution Properties vs Temperature  
1e-3mFe+5e-5mCo+5e-5mNi in 1 kg of water (open to S)



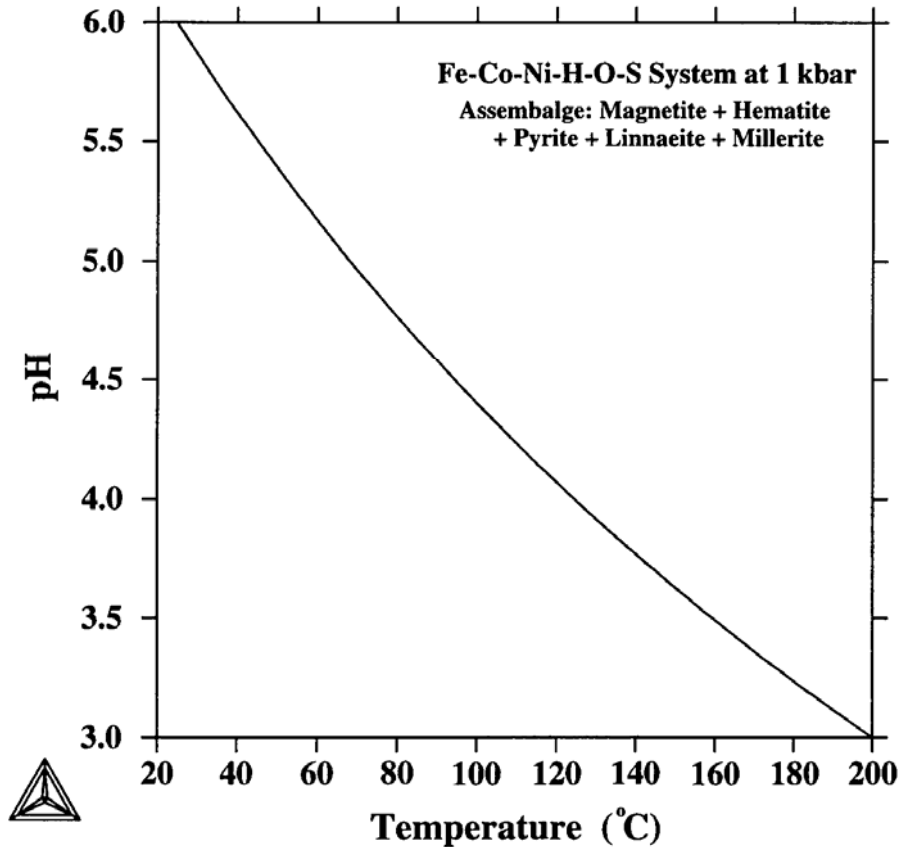
Variations of aqueous concentration, and of input amount of sulfur, with temperature for the equilibrium assemblage Magnetite-Hematite-Pyrite-Linnaeite-Millerite in the heterogeneous interaction between an Fe-Alloy (consisting of 1E-3 m Fe, 5E-5 m Co and 5E-5 m Ni) and 1 kg of water (open to S) at 1 kbar.

# Case 3: Corrosion of Steel

**THERMO-CALC: Heterogeneous Interaction**  
Aqueous Solution Properties vs Temperature  
1e-3mFe+5e-5mCo+5e-5mNi in 1 kg of water (open to S)



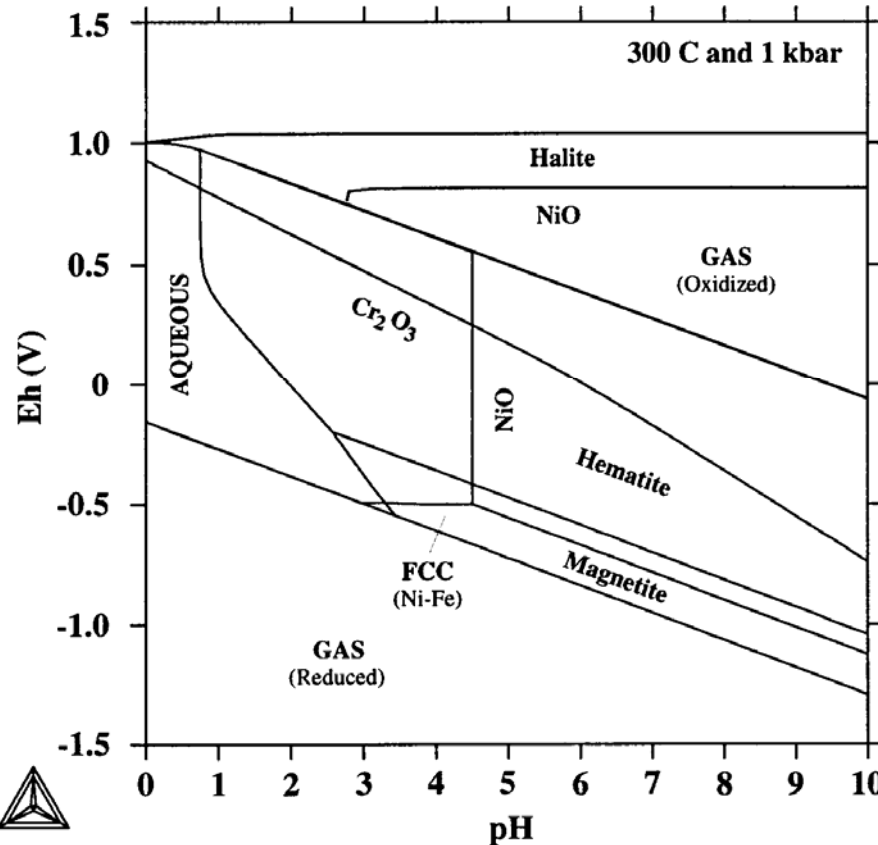
**THERMO-CALC: Heterogeneous Interaction**  
Aqueous Solution Properties vs Temperature  
1e-3mFe+5e-5mCo+5e-5mNi in 1 kg of water (open to S)



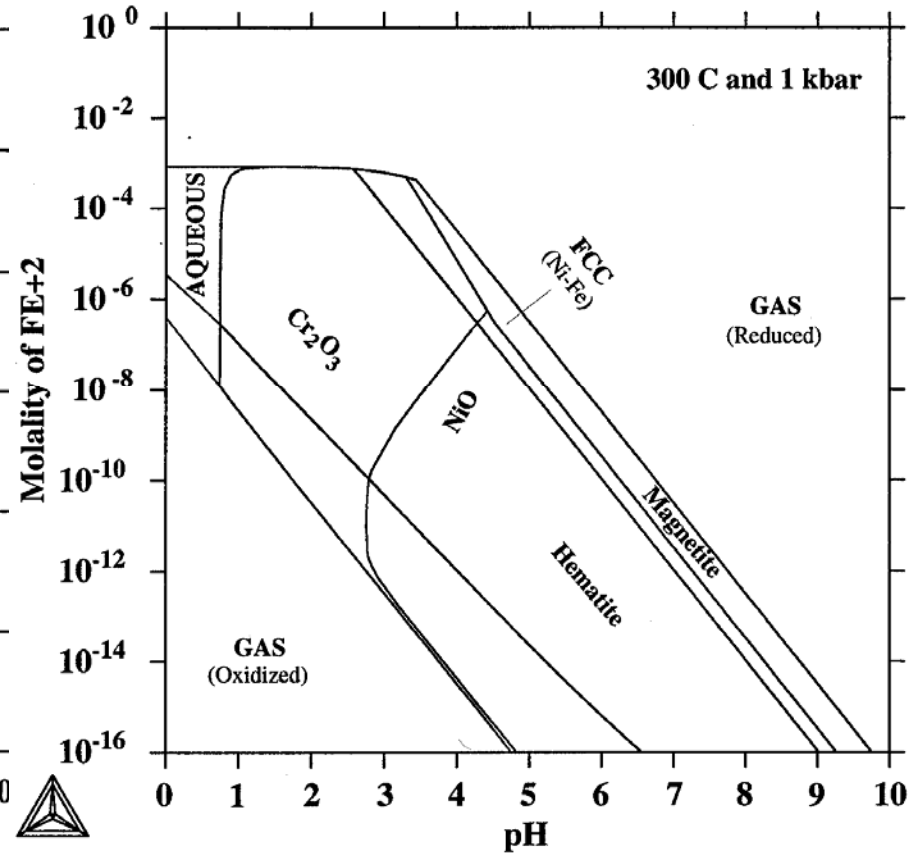
Variations of Eh and pH with temperature for the equilibrium assemblage Magnetite-Hematite-Pyrite-Linnaeite-Millerite in the heterogeneous interaction between an Fe-Alloy (consisting of 1E-3 m Fe, 5E-5 m Co and 5E-5 m Ni) and 1 kg of water (open to S) at 1 kbar.

# Case 3b Corrosion of Steel

THERMO-CALC: POURBAIX Module Calculation  
8.5e-4mFe+1e-4mCr+5e-5mNi in 1 kg of water (with 3mNaCl)



THERMO-CALC: POURBAIX Module Calculation  
8.5e-4mFe+1e-4mCr+5e-5mNi in 1 kg of water (with 3mNaCl)



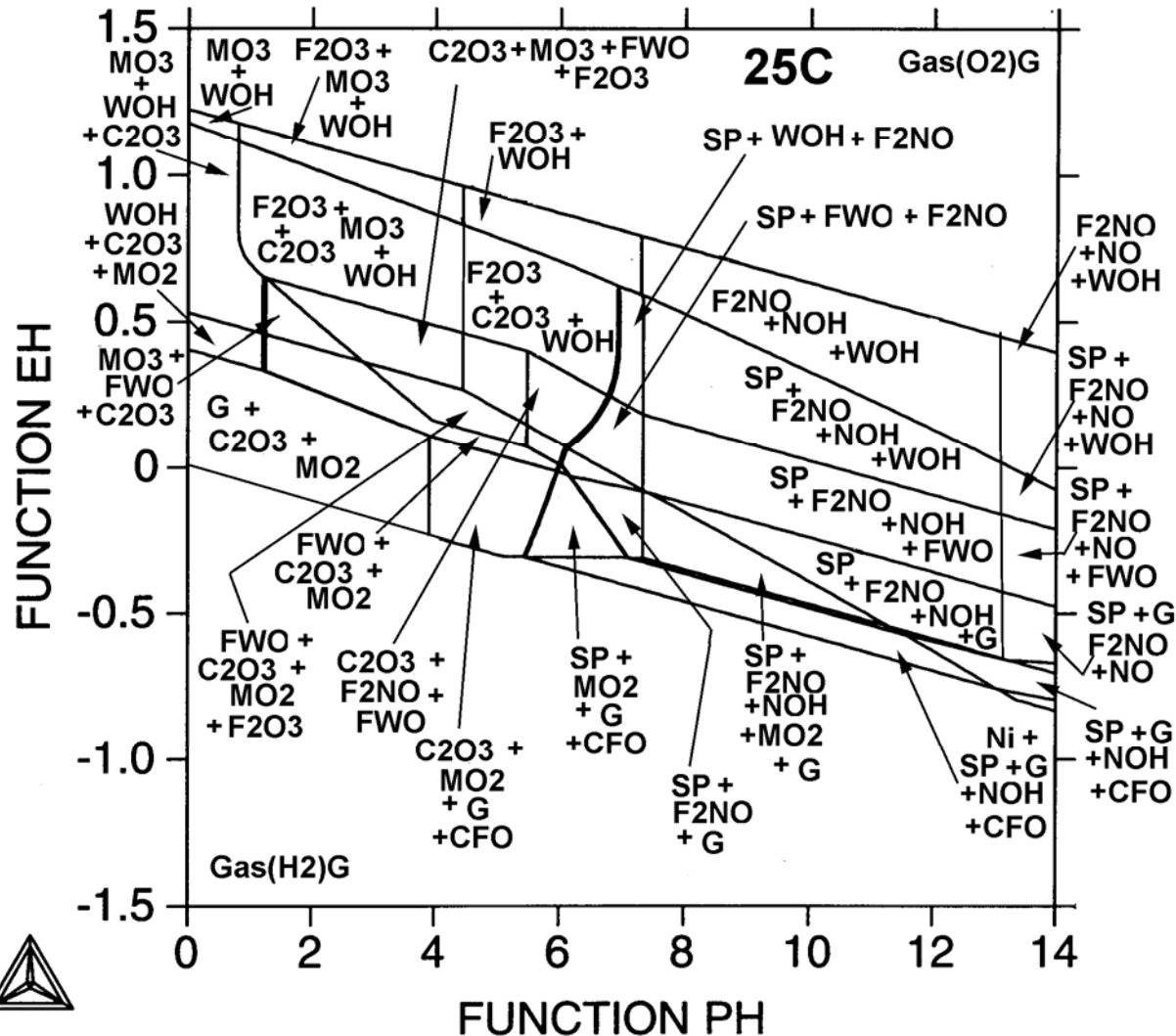
Pourbaix diagram, and Fe<sup>2+</sup> molality vs. pH diagram, for the heterogeneous interaction between an Fe-Alloy (consisting of 8.5E-4 m Fe, 1E-4 m Cr and 5E-5 m Ni) and 1 kg of water (with 3 m NaCl) at 300°C and 1 kbar.

# Case 4: Corrosion of C22 Superalloys

Fe2NiO4= F2NO Ni(OH)2=NOH WO2(OH)=WOH

NiO=NO SP=Spinel FWO=FeWO4 Cr2FeO4=CFO

MO2=MoO2 MO3=MoO3 Cr2O3=C2O3 Fe2O3=F2O3



Calculated Pourbaix diagram for 58.1Ni-21.3Cr-13.6Mo-4.0Fe-3.0W (1 gm total) in 1 kg of water at 25°C.

Larry Kaufman, 2002:  
DOE-UCRL-JC-150606

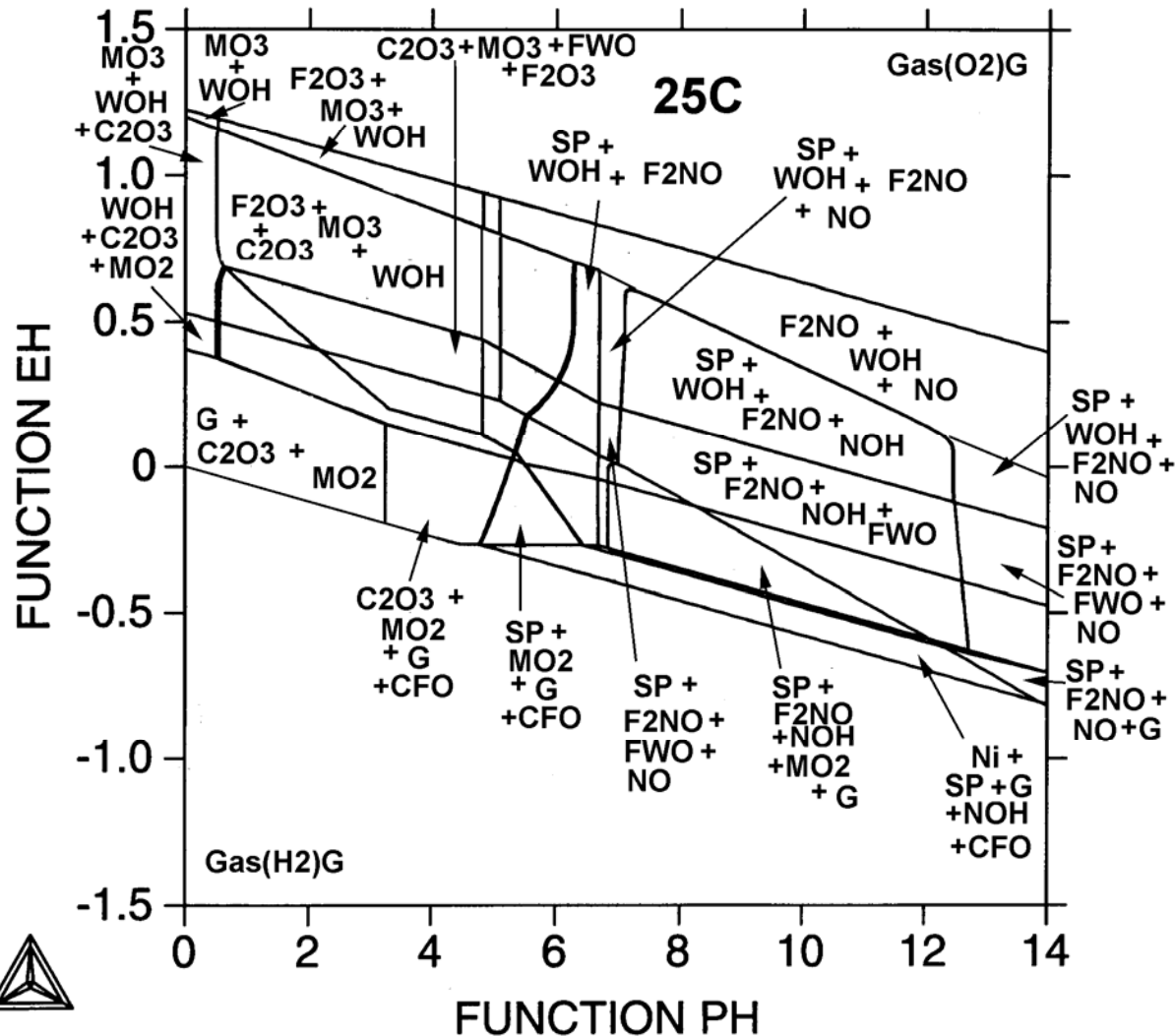


# Case 4: Corrosion of C22 Superalloys

Fe2NiO4= F2NO Ni(OH)2=NOH WO2(OH)=WOH

NiO=NO SP=Spinel FWO=FeWO4 Cr2FeO4=CFO

MO2=MoO2 MO3=MoO3 Cr2O3=C2O3 Fe2O3=F2O3



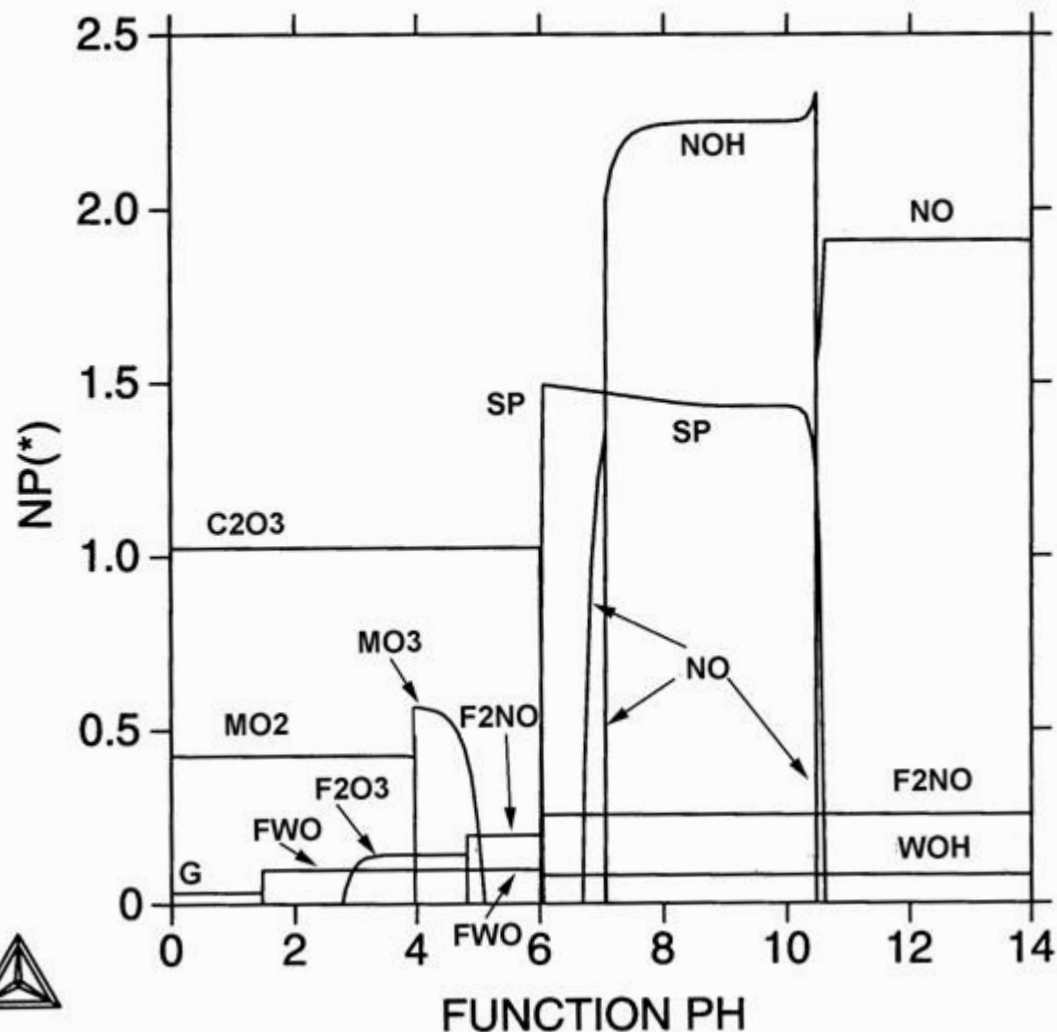
Calculated Pourbaix diagram for 58.1Ni-21.3Cr-13.6Mo-4.0Fe-3.0W (100 gm total) in 1 kg of water at 25°C.

Larry Kaufman, 2002:  
DOE-UCRL-JC-150606



# Case 4: Corrosion of C22 Superalloys

Fe<sub>2</sub>NiO<sub>4</sub>= F2NO Ni(OH)<sub>2</sub>=NOH WO<sub>2</sub>(OH)=WOH  
NiO=NO SP=Spinel FWO=FeWO<sub>4</sub> Cr<sub>2</sub>FeO<sub>4</sub>=CFO  
MO<sub>2</sub>=MoO<sub>2</sub> MO<sub>3</sub>=MoO<sub>3</sub> Cr<sub>2</sub>O<sub>3</sub>=C2O3 Fe<sub>2</sub>O<sub>3</sub>=F2O3



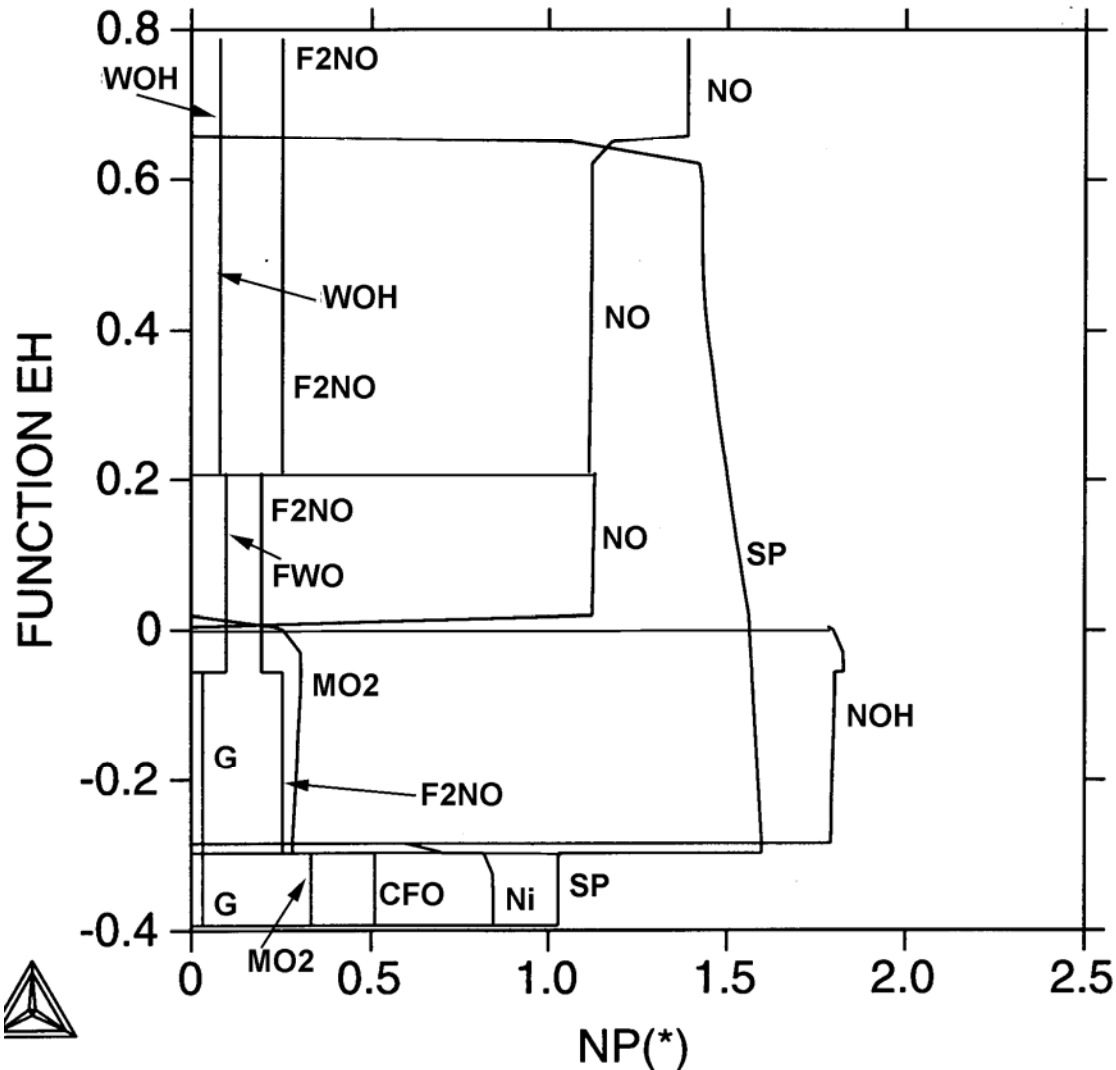
Calculated Pourbaix diagram for 58.1Ni-21.3Cr-13.6Mo-4.0Fe-3.0W (100 gm total) in 1 kg of water at 25°C.

Larry Kaufman, 2002:  
DOE-UCRL-JC-150606



# Case 4: Corrosion of C22 Superalloys

Fe2NiO4= F2NO Ni(OH)2=NOH WO2(OH)=WOH  
NiO=NO SP=Spinel FWO=FeWO4 Cr2FeO4=CFO  
MO2=MoO2 MO3=MoO3 Cr2O3=C2O3 Fe2O3=F2O3



Calculated Pourbaix diagram for 58.1Ni-21.3Cr-13.6Mo-4.0Fe-3.0W (100 gm total) in 1 kg of water at 25°C.

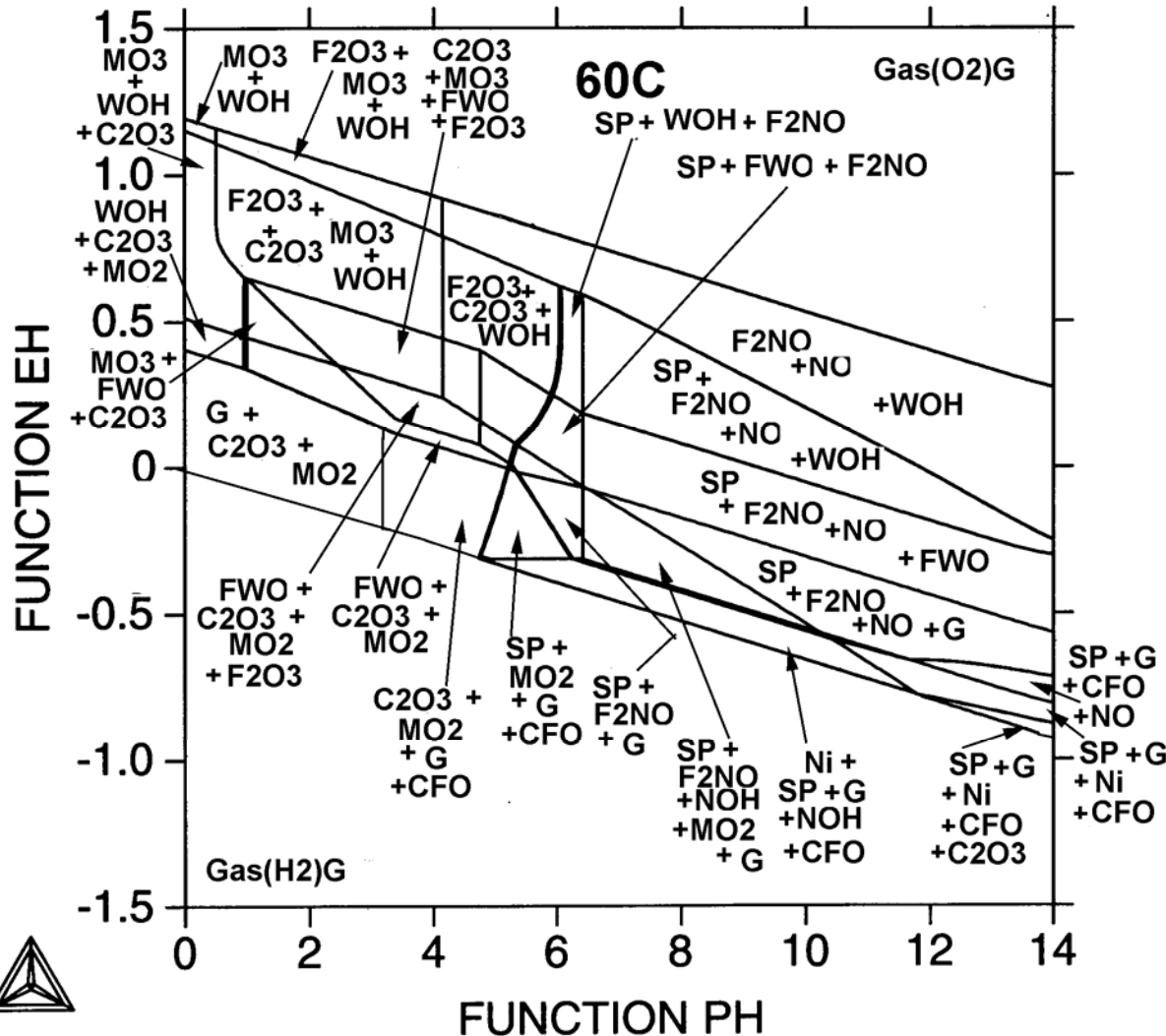
Larry Kaufman, 2002:  
DOE-UCRL-JC-150606

# Case 4: Corrosion of C22 Superalloys

Fe2NiO4= F2NO Ni(OH)2=NOH WO2(OH)=WOH

NiO=NO SP=Spinel FWO=FeWO4 Cr2FeO4=CFO

MO2=MoO2 MO3=MoO3 Cr2O3=C2O3 Fe2O3=F2O3

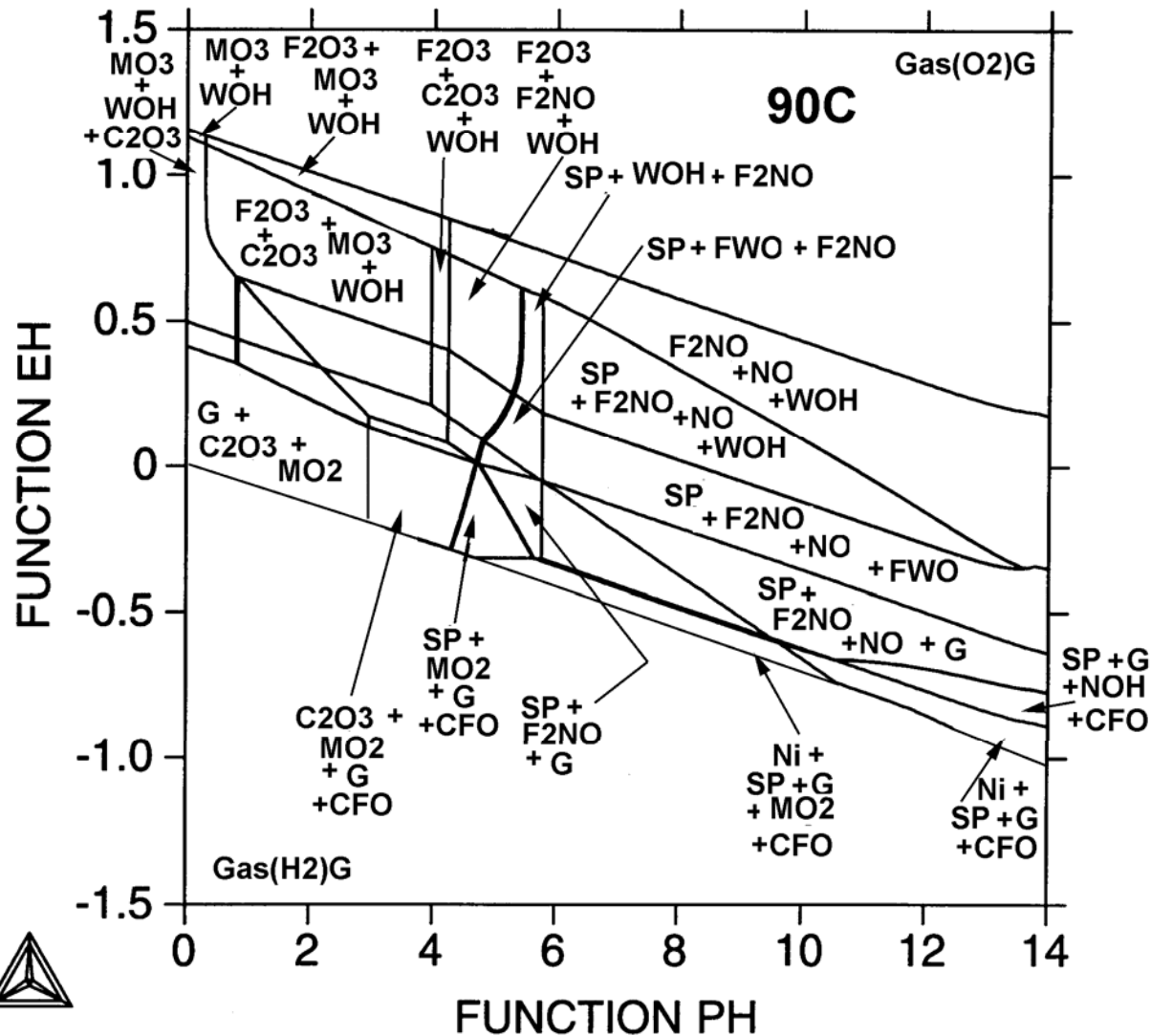


Calculated Pourbaix diagram for 58.1Ni-21.3Cr-13.6Mo-4.0Fe-3.0W (1 gm total) in 1 kg of water at 60°C.

Larry Kaufman, 2002:  
DOE-UCRL-JC-150606

# Case 4: Corrosion of C22 Superalloys

$\text{Fe}_2\text{NiO}_4 = \text{F}_2\text{NO}$     $\text{Ni}(\text{OH})_2 = \text{NOH}$     $\text{WO}_2(\text{OH}) = \text{WOH}$   
 $\text{NiO} = \text{NO}$     $\text{SP} = \text{Spinel}$     $\text{FWO} = \text{FeWO}_4$     $\text{Cr}_2\text{FeO}_4 = \text{CFO}$   
 $\text{MO}_2 = \text{MoO}_2$     $\text{MO}_3 = \text{MoO}_3$     $\text{Cr}_2\text{O}_3 = \text{C}_2\text{O}_3$     $\text{Fe}_2\text{O}_3 = \text{F}_2\text{O}_3$



Calculated Pourbaix diagram for 58.1Ni-21.3Cr-13.6Mo-4.0Fe-3.0W (1 gm total) in 1 kg of water at 90°C.

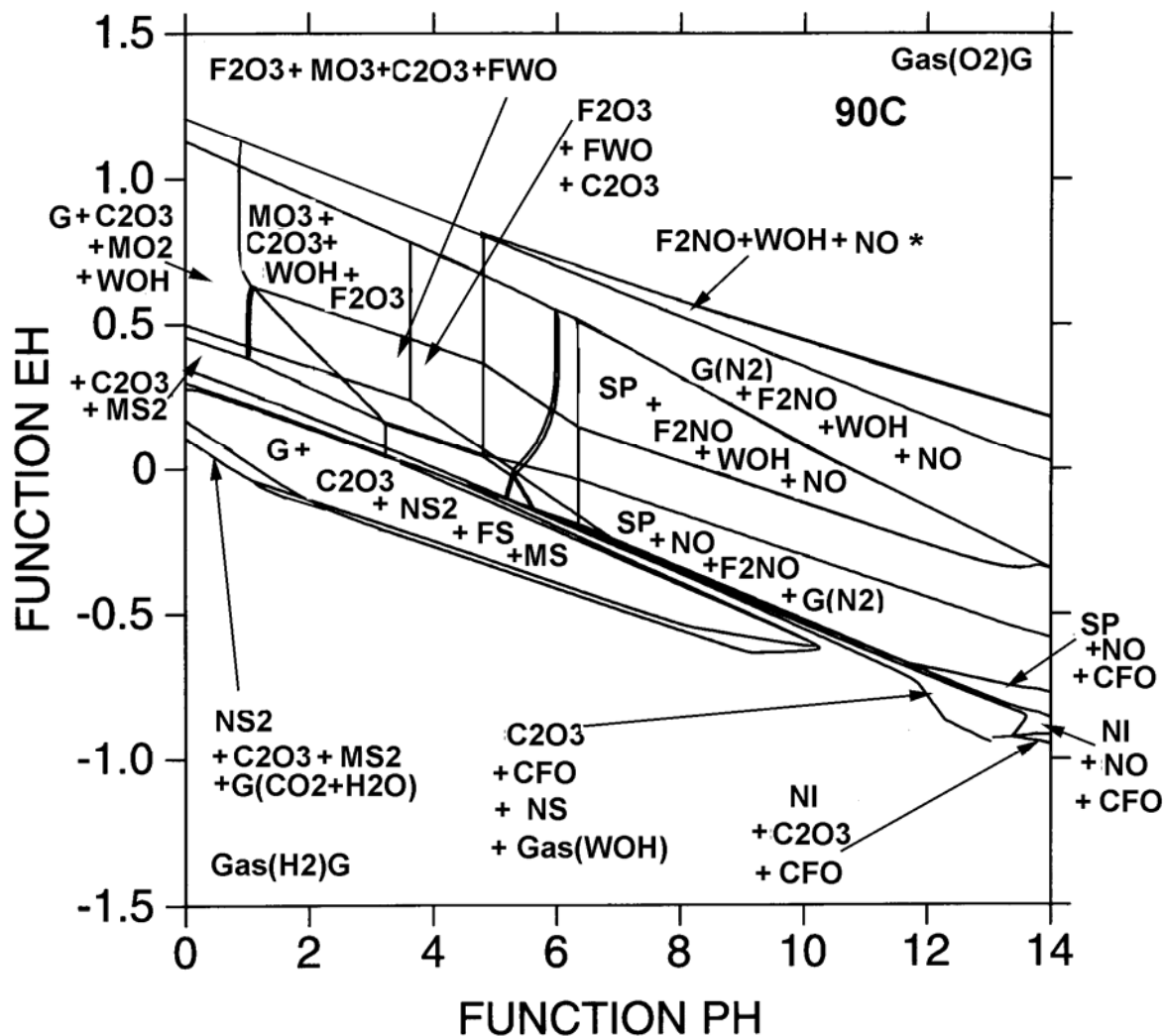
*Larry Kaufman, 2002: DOE-UCRL-JC-150606*





# Case 4: Corrosion of C22 Superalloys

FeS2=FS NiS=NS NiS2=NS2 MoS2=MS KNO=KNO3  
 Fe2NiO4= F2NO Ni(OH)2=NOH WO2(OH)=WOH NI=NI  
 NiO=NO SP=Spinel FWO=FeWO4 Cr2FeO4=CFO  
 MO2=MoO2 MO3=MoO3 Cr2O3=C2O3 Fe2O3=F2O3



Calculated Pourbaix diagram for 58.1Ni-21.3Cr-13.6Mo-4.0Fe-3.0W (1 gm total) in Basic Acidic Water (BAW) at 90°C.

The BAW contains 1000 gms of H<sub>2</sub>O, 23.0 gms of NO<sub>3</sub><sup>-1</sup>, 1,37.6 gms of Na<sup>+1</sup>, 24.25 gms of Cl<sup>-1</sup> and 38.6 gms of SO<sub>4</sub><sup>-2</sup>. The following components of SAW were not included: 1.0 gms. of Ca<sup>+2</sup>, 3.4 gms of K<sup>+1</sup>, 0.058 gms of SiO<sub>2</sub>, and 1.0 gms of Mg<sup>+2</sup>. The entire space is covered by an aqueous solution and a gas phase whose composition varies except for the regions noted with asterisks(\*) in which there is no gas phase.

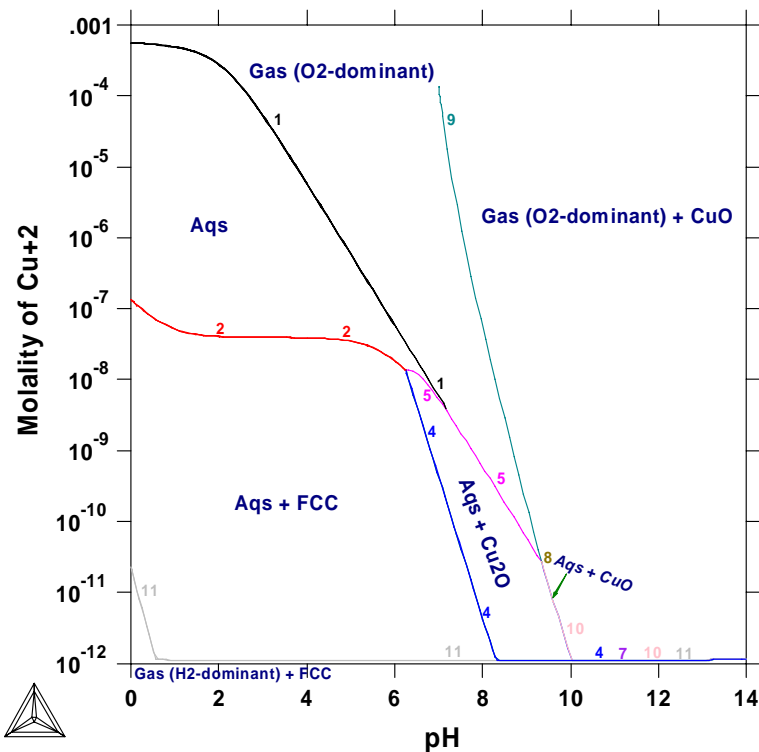
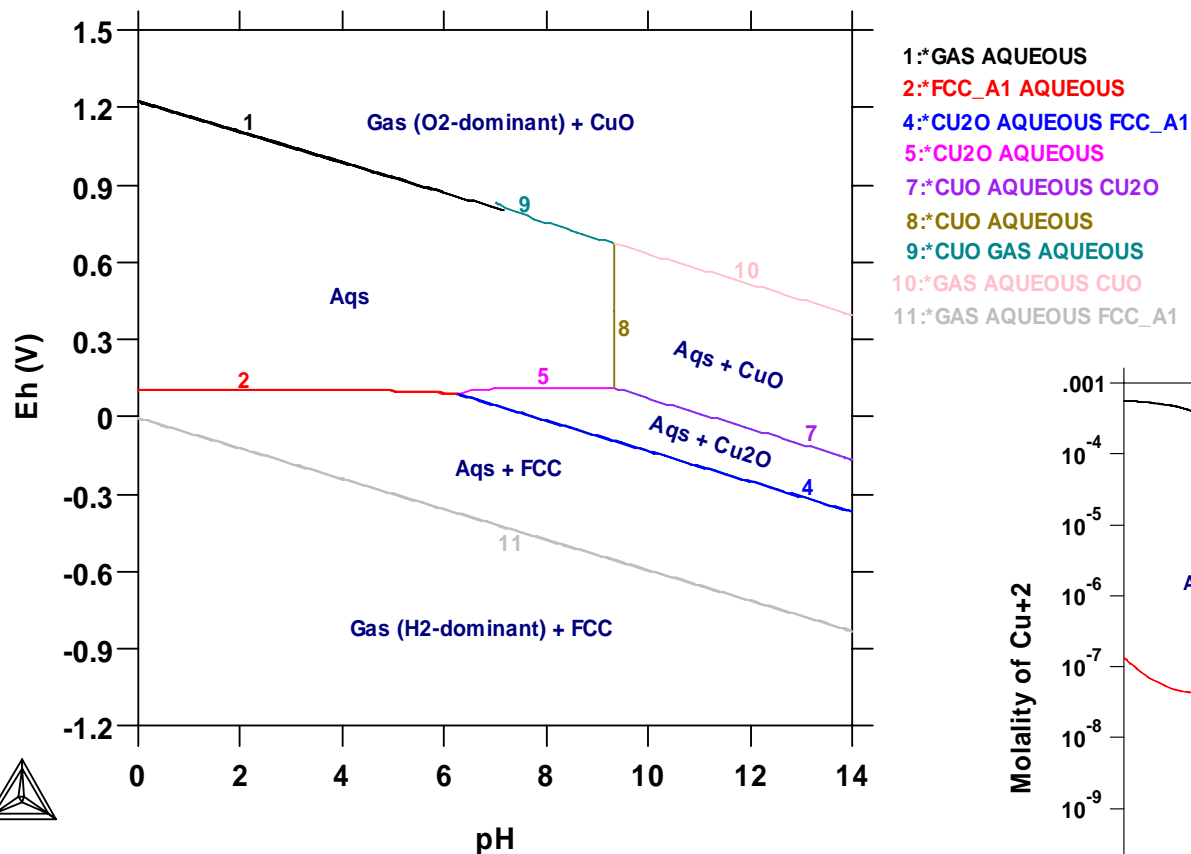
Larry Kaufman, 2002: DOE-UCRL-JC-150606

# Case 5: Corrosion of Cu-40Zn Alloy

THERMO-CALC (2004.03.23): Pourbaix Diagram

Databases: TCAQ2 + SSUB3 + SSOL2

0.001 m Cu-40wt%Zn alloy in 1 kg of water (with 0.1 m NaCl) at 25 C and 1 bar

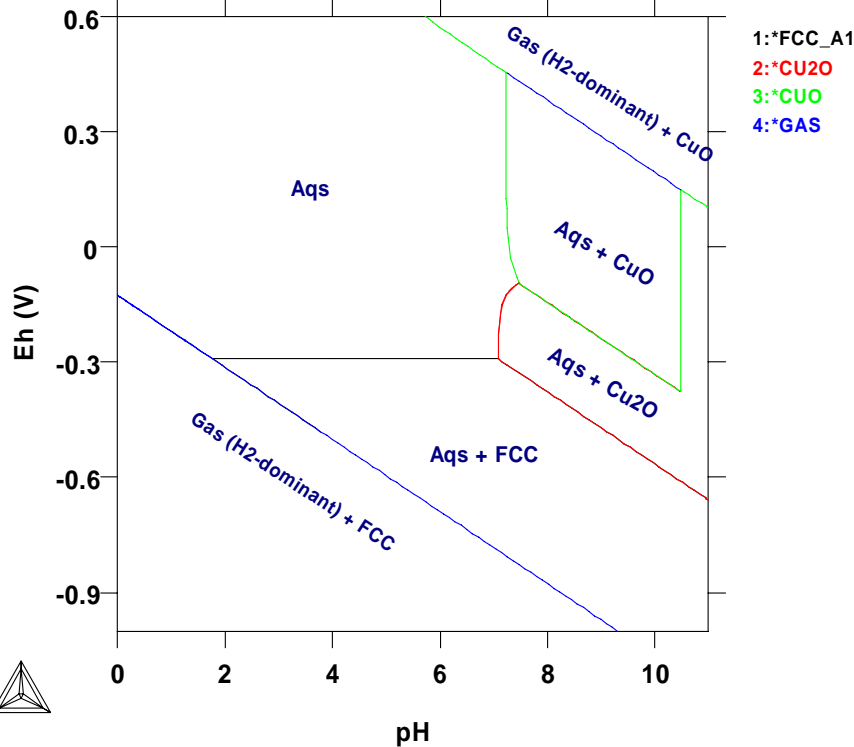


Calculated Pourbaix Diagram and related variation of  $m(\text{Cu}^{+2})$  property for 0.001 mole Cu-40wt%Zn Alloy in 1 kg of Water (with 0.1 m NaCl) at 25°C and 1 bar.

# Case 5: Corrosion of Cu-40Zn Alloy

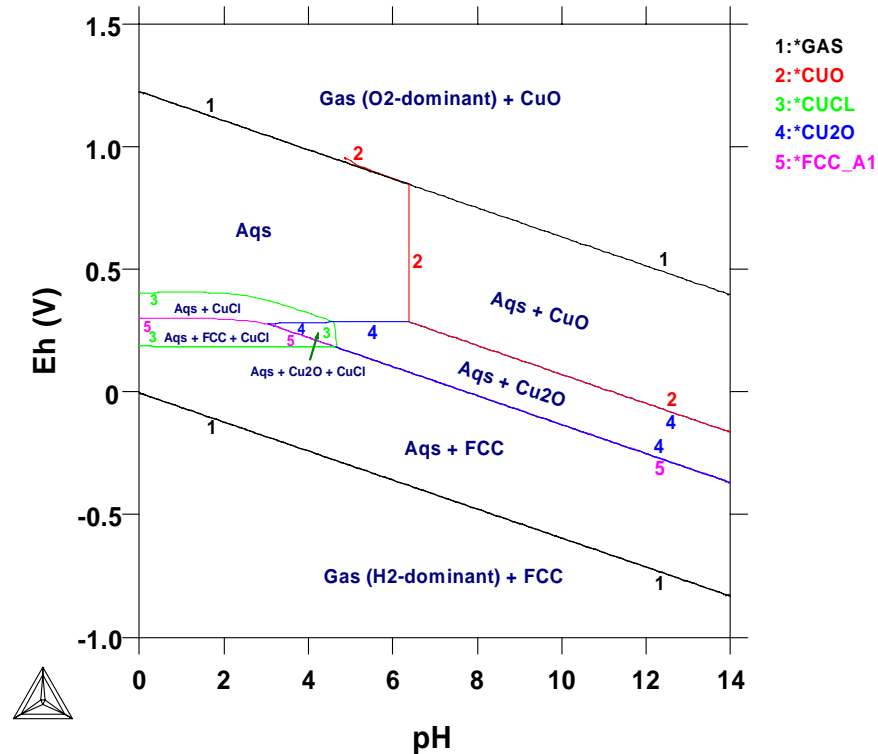
THERMO-CALC (2004.03.23): Pourbaix Diagram  
Databases: TCAQ2 + SSUB3 + SSOL2

0.001 m Cu-40wt%Zn alloy in 1 kg of water (with 0.1 m NaCl) at 200 C & 500 bar



THERMO-CALC (2004.03.23): Pourbaix Diagram  
Databases: TCAQ2 + SSUB3 + SSOL2

1 mole Cu-40wt%Zn alloy in 1 kg of water (with 0.1 m NaCl) at 25 C and 1 bar



Calculated Pourbaix Diagram for 0.001 mole Cu-40wt%Zn Alloy in 1 kg of Water (with 0.1 m NaCl) at 200°C and 100 bar.

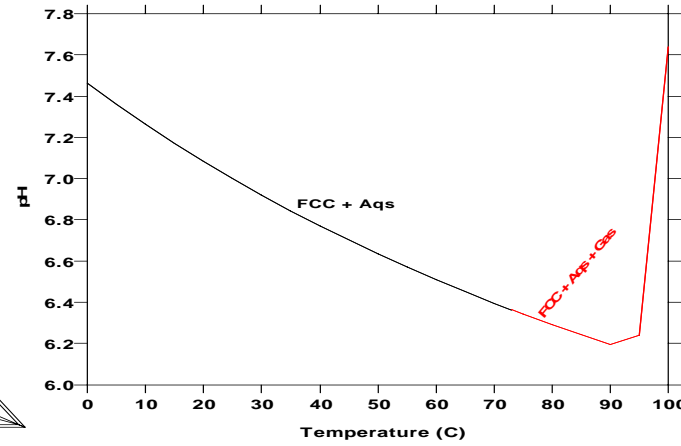
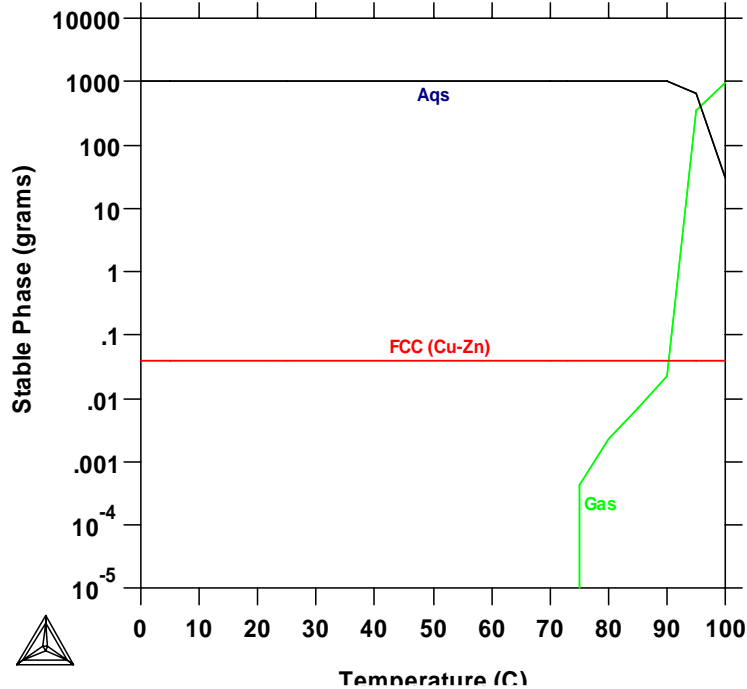
Calculated Pourbaix Diagram for 1 mole Cu-40wt%Zn Alloy in 1 kg of Water (with 0.1 m NaCl) at 25°C and 1 bar.

# Case 5: Corrosion of Cu-40Zn Alloy

Calculated Property Diagrams for 0.001 mole Cu-40wt%Zn Alloy in 1 kg of Water (with 0.1 m NaCl) at 1 bar and varied temperatures.

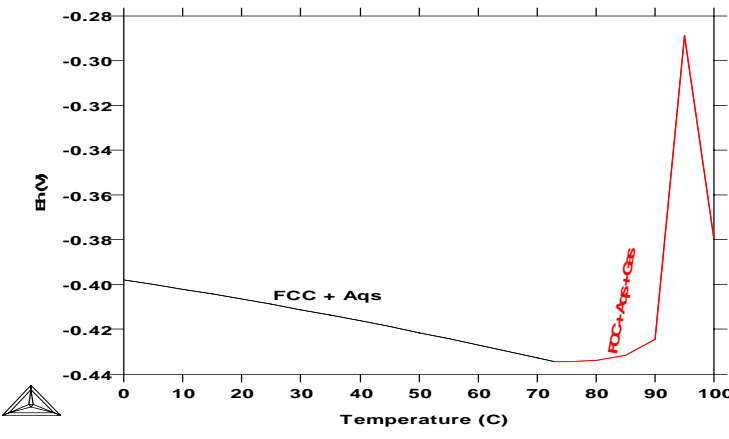
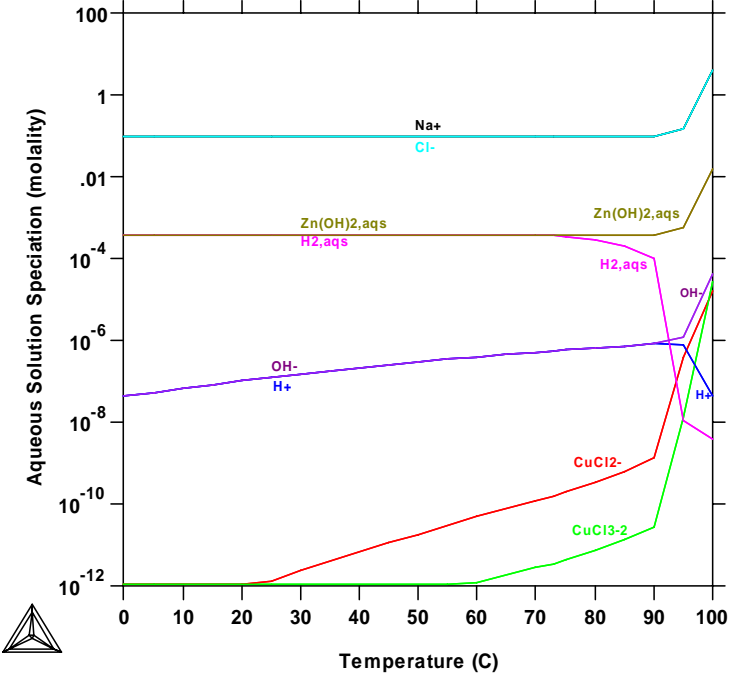
THERMO-CALC (2004.03.23): Property Diagram  
 Databases: TCAQ2 + SSUB3 + SSOL2

0.001 m Cu-40wt%Zn alloy in 1 kg of water (with 0.1 m NaCl) at 1 bar



THERMO-CALC (2004.03.23): Property Diagram  
 Databases: TCAQ2 + SSUB3 + SSOL2

0.001 m Cu-40wt%Zn alloy in 1 kg of water (with 0.1 m NaCl) at 1 bar

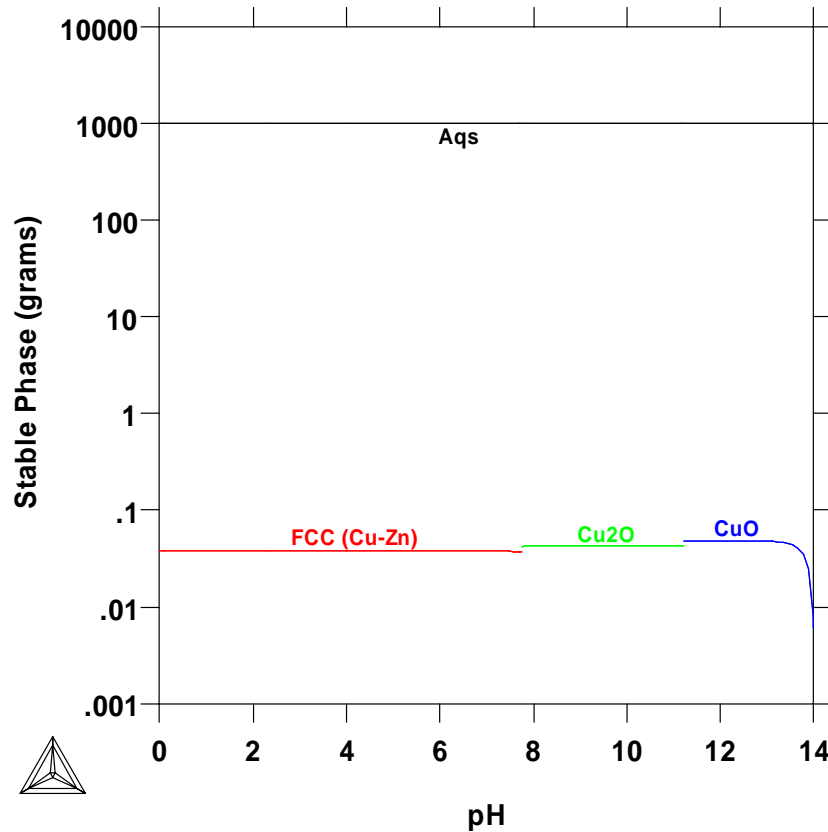


# Case 5: Corrosion of Cu-40Zn Alloy

THERMO-CALC (2004.03.23): Property Diagram

Databases: TCAQ2 + SSUB3 + SSOL2

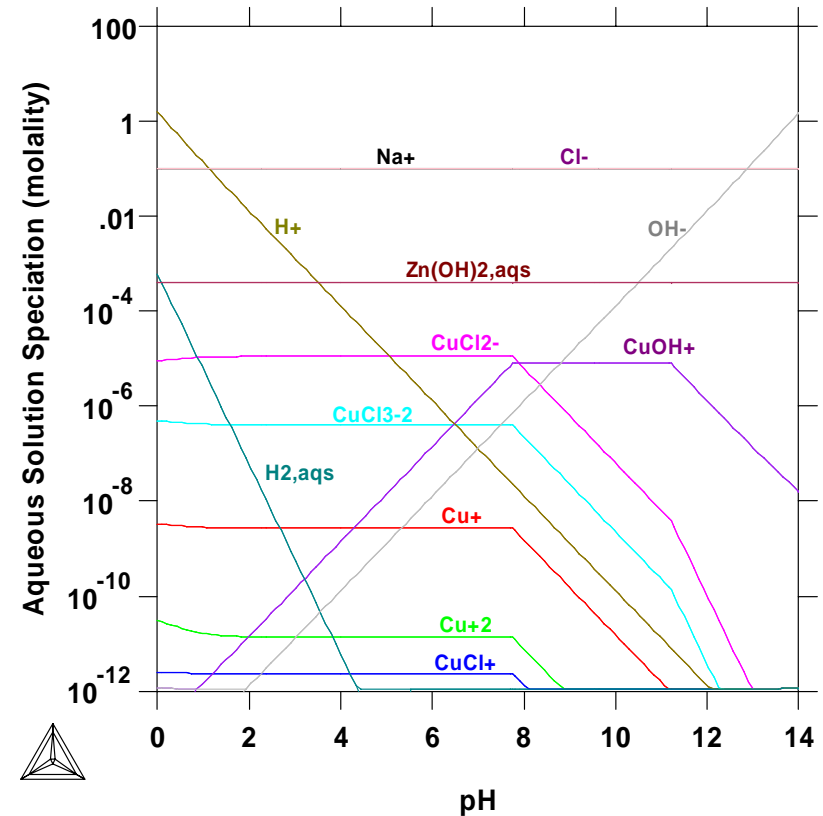
0.001 m Cu-40wt%Zn alloy in 1 kg of water (with 0.1 m NaCl) at 1 bar & zero Eh



THERMO-CALC (2004.03.23): Property Diagram

Databases: TCAQ2 + SSUB3 + SSOL2

0.001 m Cu-40wt%Zn alloy in 1 kg of water (with 0.1 m NaCl) at 1 bar & zero Eh



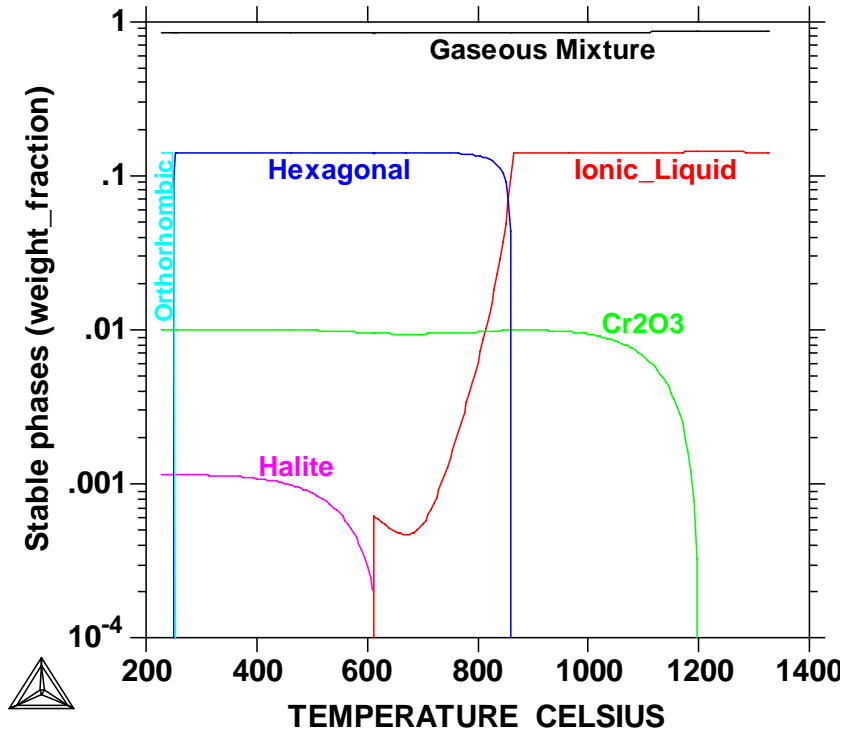
Calculated Property Diagrams for 0.001 mole Cu-40wt%Zn Alloy in 1 kg of Water (with 0.1 m NaCl) at 25°C, 1 bar, zero Eh and varied acidity.

# Salt Corrosion

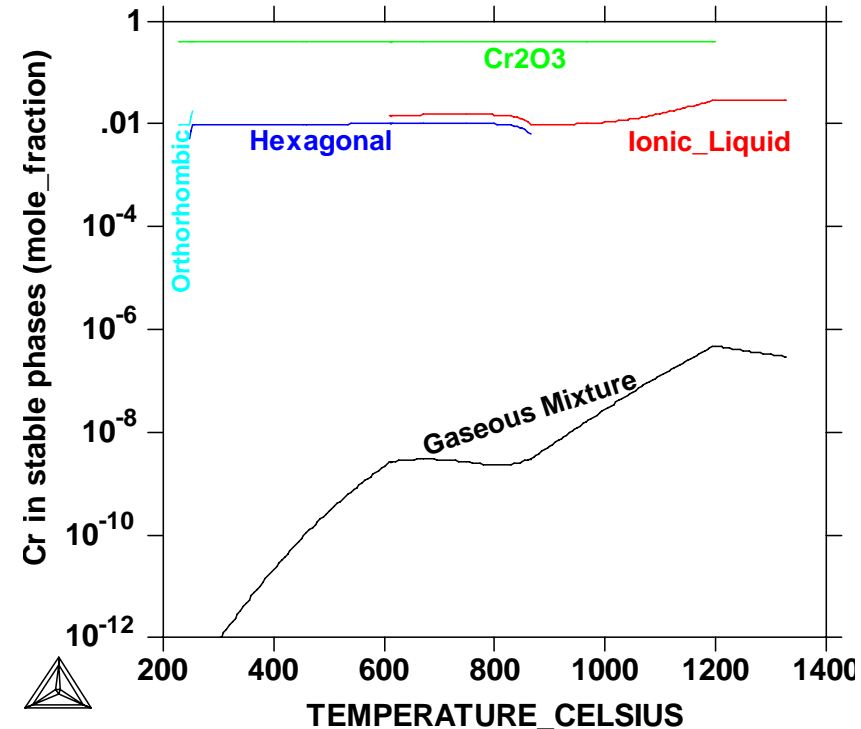
## Example: Salt Corrosion of Alloy Surface

Using the SALT database (and/or in a combination with other databases), one can calculate various types of phase diagrams and property diagrams for heterogeneous interaction systems/processes involving molten salts.

**Corrosion of Cr<sub>2</sub>O<sub>3</sub> in C-H-O-S-N-Na-Cl environment**



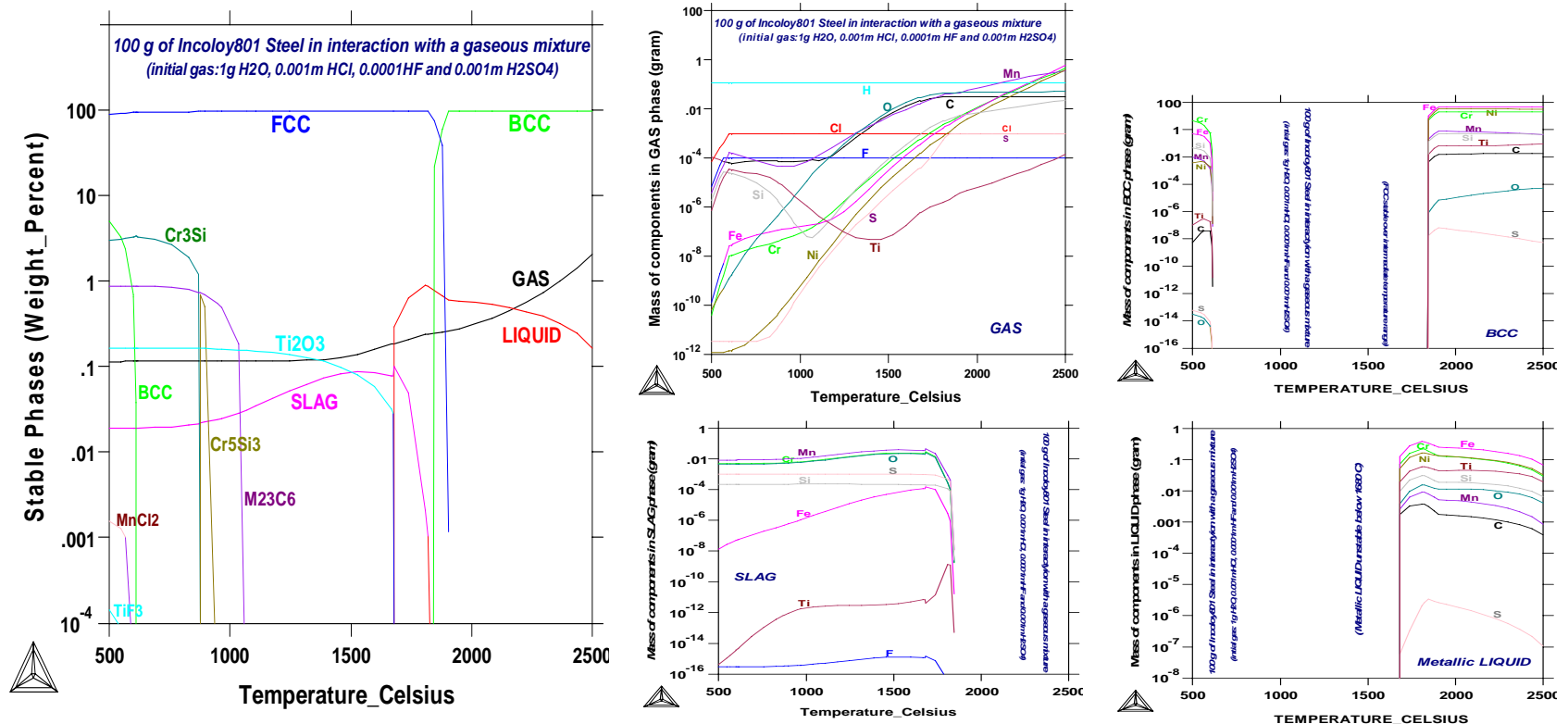
**Corrosion of Cr<sub>2</sub>O<sub>3</sub> in C-H-O-S-N-Na-Cl environment**



As a typical form in the oxide layer on the surface of stainless steels, Ni-based superalloys, etc, Cr<sub>2</sub>O<sub>3</sub> provides a protection from corrosion attacks by hot or molten salts, high-temperature gases, or aqueous solutions. This calculation illustrates that under certain aggressive conditions, the Cr<sub>2</sub>O<sub>3</sub> layer may be dissolved by the attacking salts, and thus the applied alloy may be exposed to further corrosion attacks from oxidizing and sulphidising environments.

## Example: High-Temperature (Gaseous) Corrosion of Alloys

Using the TCMP2 or SSUB3 database (and/or in a combination with other alloy databases), one can calculate various types of phase diagrams and property diagrams for heterogeneous interaction systems/processes involving gaseous mixtures.



Calculated property diagrams of the heterogeneous interaction between 100 g of Incoloy 801 steel (wrought Fe-based superalloy with a composition of Fe44.5-Ni32-Cr20.5-Ti1.1-Mn0.8-Si0.5-C0.05 wt%) and a gas mixture (of 1 g H<sub>2</sub>O, 0.001 m HCl, 0.0001 m HF and 0.001 m H<sub>2</sub>SO<sub>4</sub>). The calculation shows that the gas mixture will dissolve the steel components (especially with increasing temperatures), meanwhile LIQUID phase or SLAG+Ti<sub>2</sub>O<sub>3</sub> phases may form during the interaction over certain temperature ranges.

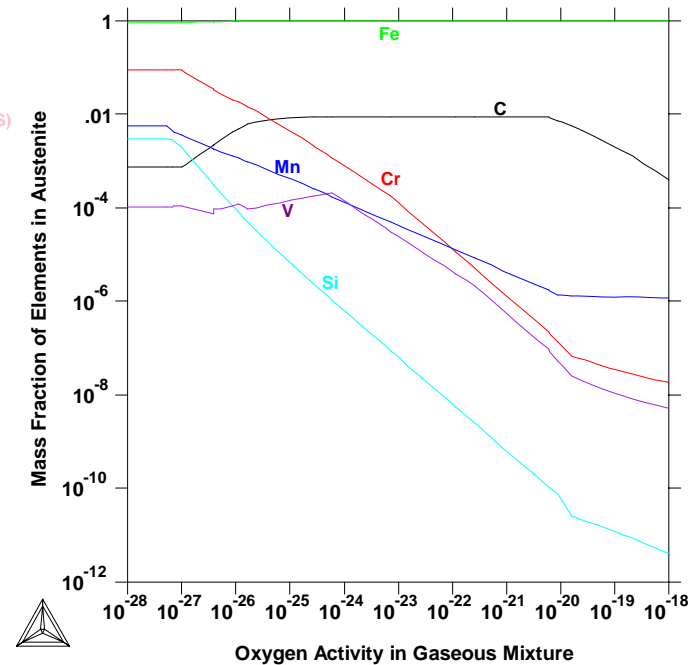
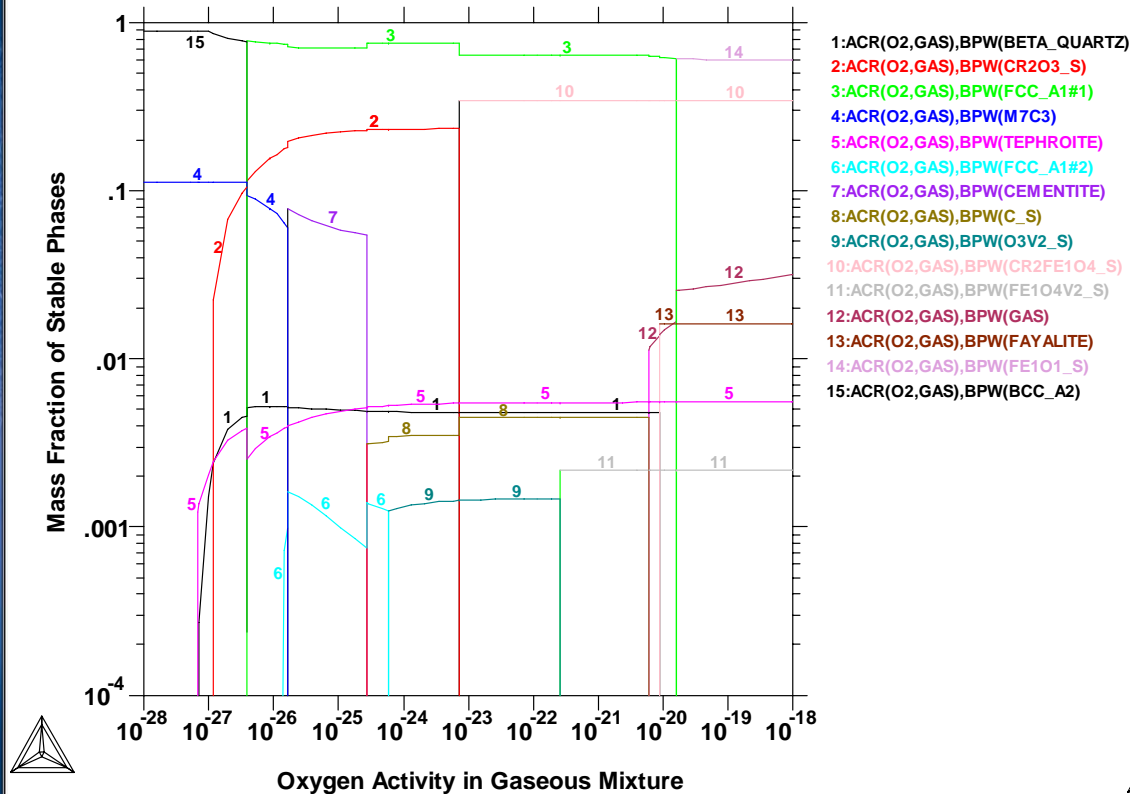
# Surface Redox Reactions (I)

## Example: Formation of Oxide Layer on Steel Surface: Protection against corrosion

THERMO-CALC (2008.05.22:17.49) : Formation of Oxide Layer on Steel Surface

DATABASE: TCFe6

$P=100000$ ,  $T=1073$ ,  $B=100$ ,  $B(\text{Cr})=16.$ ,  $B(\text{V})=1\text{E}-1$ ,  $B(\text{C})=1.$ ,  $B(\text{Mn})=3\text{E}-1$ ,  $B(\text{Si})=3\text{E}-1$

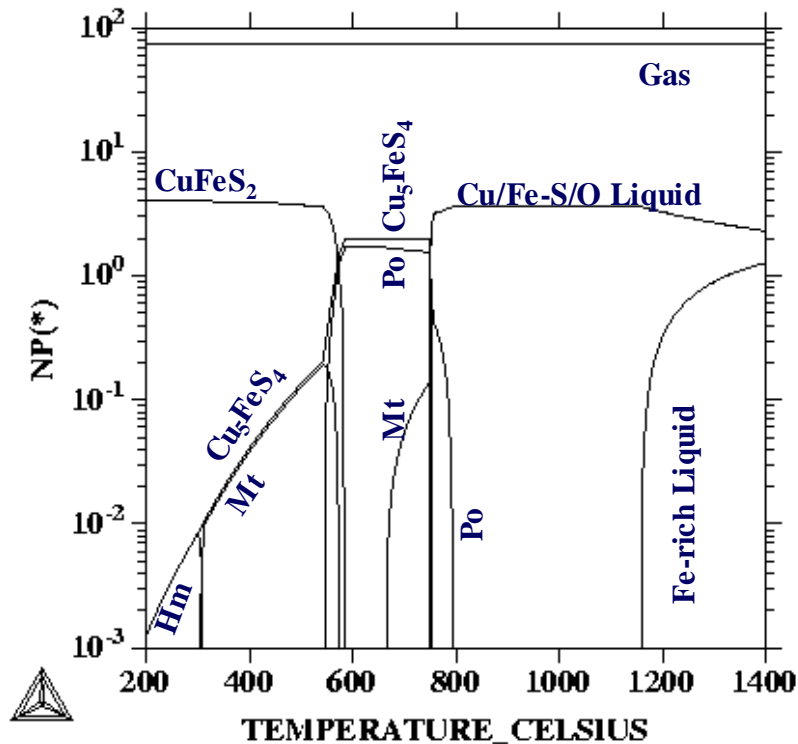


Stable phases and element distribution of remaining austenite during the surface oxidation of the Fe-16Cr-0.3Mn-0.3Si-0.01V-1C (wt%) steel at 800°C, as a function of oxygen activity in the atmosphere.

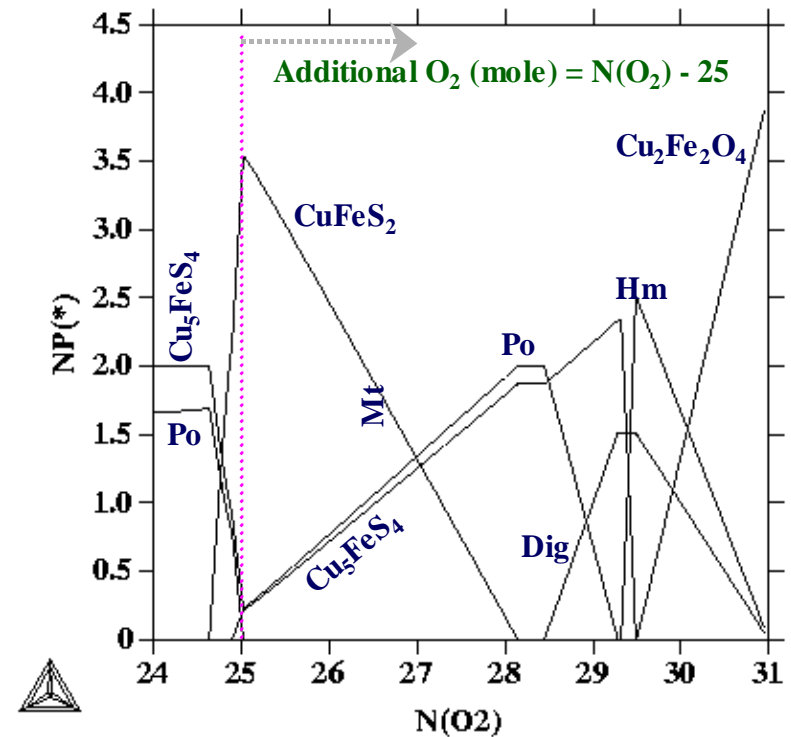
# Surface Redox Reactions (II)

## Example: Oxidation of Sulfides (CuFeS<sub>2</sub>)

Using the ION database, one can calculate various types of phase diagrams and property diagrams for oxidation processes of multiple-metal sulfides (e.g., CuFeS<sub>2</sub>, FeS<sub>2</sub>) or mixtures (e.g., CuFeS<sub>2</sub>-FeS<sub>2</sub>), to find optimal temperatures and initial bulk compositions (especially the additional oxygen input).



Stable phases during oxidation of CuFeS<sub>2</sub>, as a function of the temperature condition. The calculation is made for an interaction system of 2 moles CuFeS<sub>2</sub> and 50 moles of vapour, at 1 bar and various temperatures (200 to 1400°C).



Stable phases during oxidation of CuFeS<sub>2</sub>, varied with the additional oxygen amount. The calculation is made for an interaction system of 2 moles CuFeS<sub>2</sub> and 50 moles of vapour, at 550°C, 1 bar and various additional amounts of O<sub>2</sub>.

# Surface Redox Reactions (III)

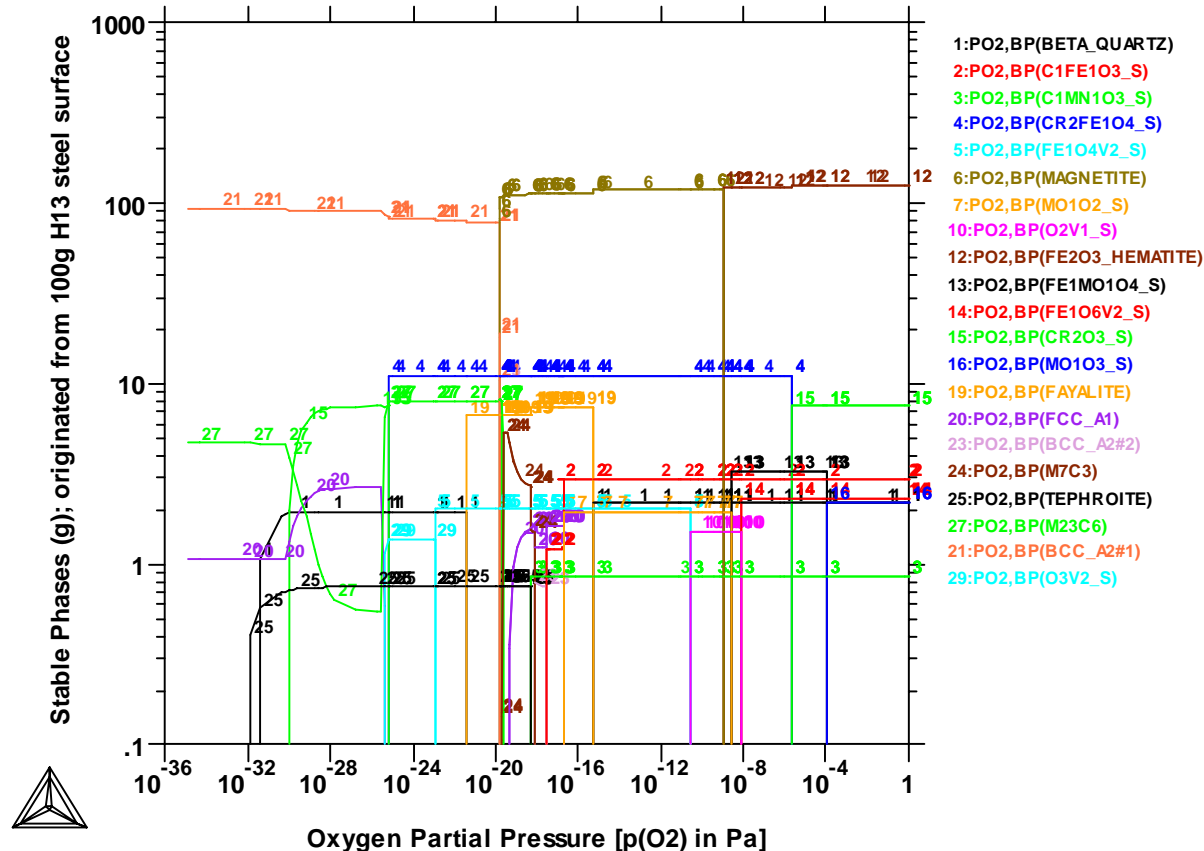
## Example: Oxidation of H13 Hot Work Steel

THERMO-CALC (2008.02.29:16.47) :

DATABASE:SSOL4

P=1E5, T=873.15, B(Fe)=90.63, B(Cr)=5.14, B(Mn)=0.41, B(Si)=1.02, B(C)=0.4,

B(V)=0.93, B(Mo)=1.46, B(S)=1E-3, B(P)=9E-3;



Stable phases during oxidation of H13 Hot Work Steel [Fe-5.14Cr-0.41Mn-1.02Si-0.40C-0.93V-1.46Mo-0.001S-0.009P-O], varied with the oxygen partial pressure. The calculation is made for an interaction system at temperature of 600°C and a total pressure of 1 bar.

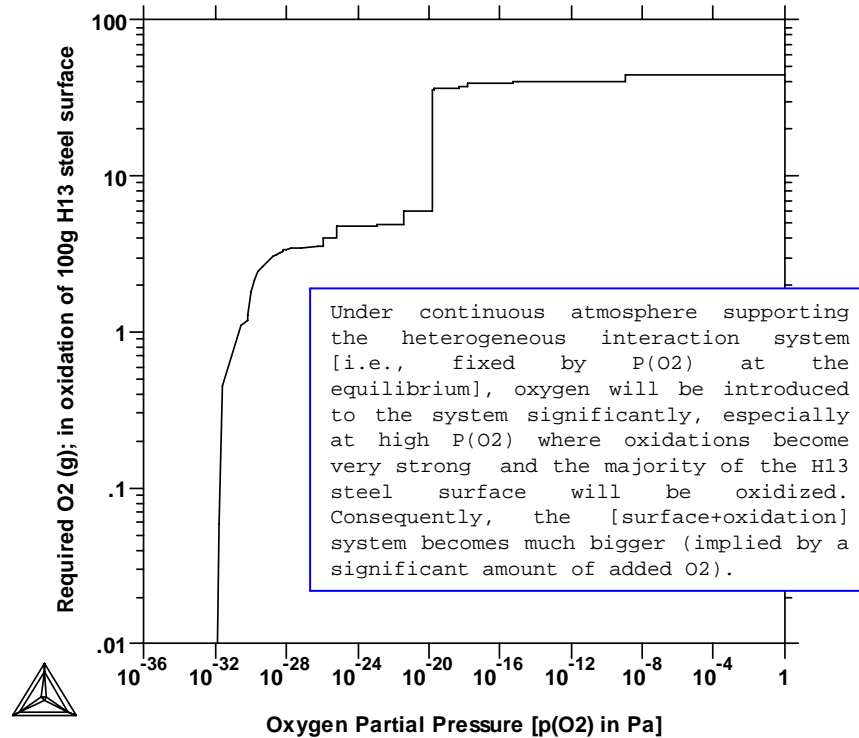
# Surface Redox Reactions (III)

## Example: Oxidation of H13 Hot Work Steel

THERMO-CALC (2008.02.29:16.16) :

DATABASE:SSOL4

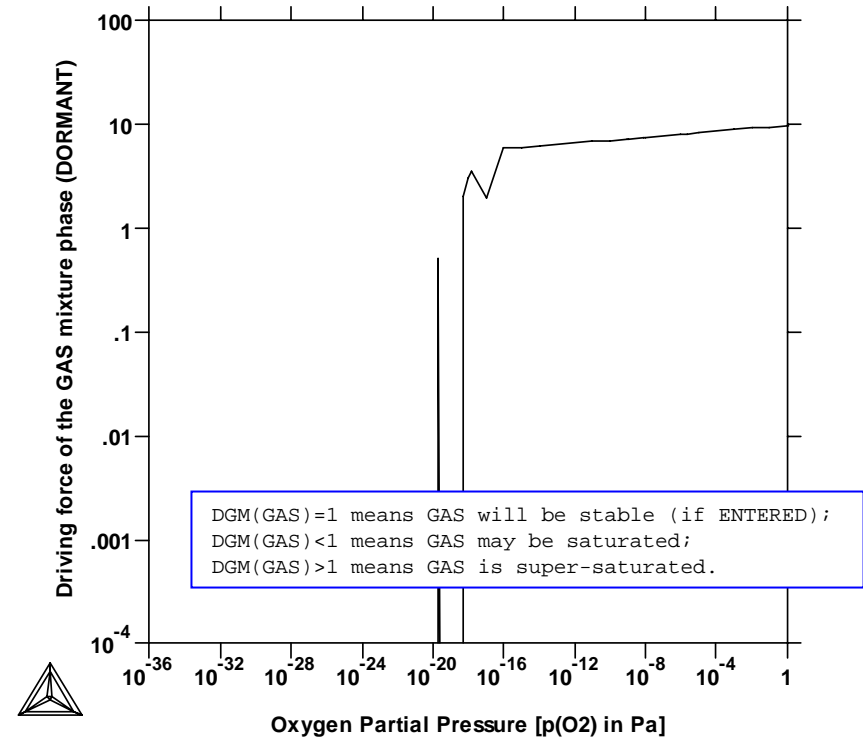
P=1E5, T=873.15, B(FE)=92.3, B(CR)=5, B(MN)=0.3, B(SI)=1, B(C)=0.4, B(V)=1;



THERMO-CALC (2008.02.29:16.16) :

DATABASE:SSOL4

P=1E5, T=873.15, B(FE)=92.3, B(CR)=5, B(MN)=0.3, B(SI)=1, B(C)=0.4, B(V)=1;



Required  $O_2$  Input and Driving force of the dormant GAS phase during oxidation of H13 Hot Work Steel [Fe-5.14Cr-0.41Mn-1.02Si-0.40C-0.93V-1.46Mo-0.001S-0.009P-O], varied with the oxygen partial pressure. The calculation is made for an interaction system at temperature of 600°C and a total pressure of 1 bar.

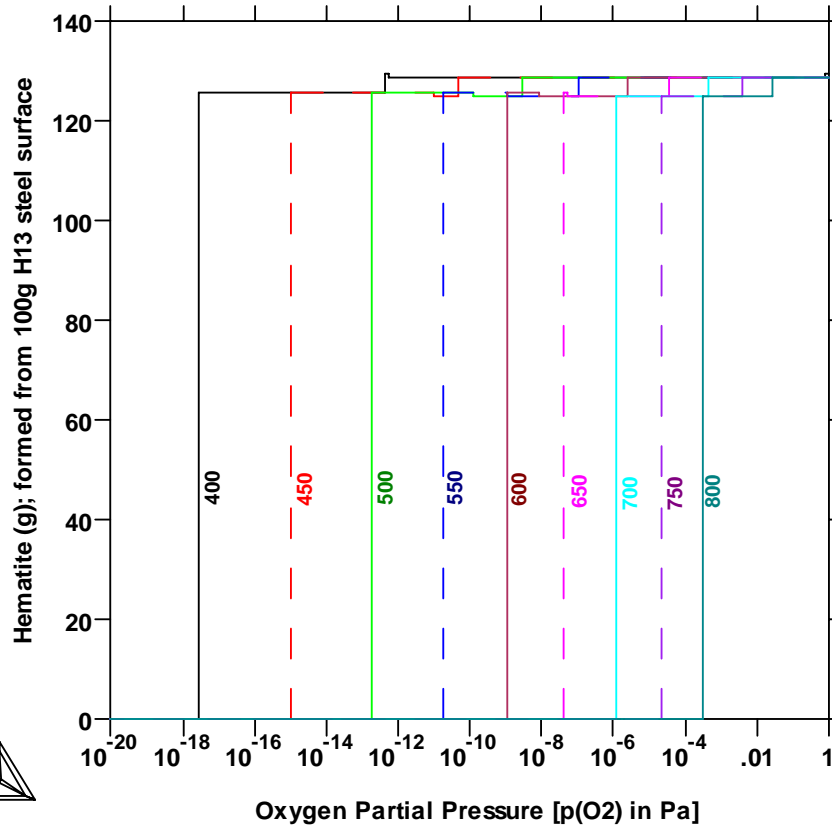
# Surface Redox Reactions (III)

## Example: Oxidation of H13 Hot Work Steel

THERMO-CALC (2008.05.22:09.32) :

Databases: SSOL4+SSUB4

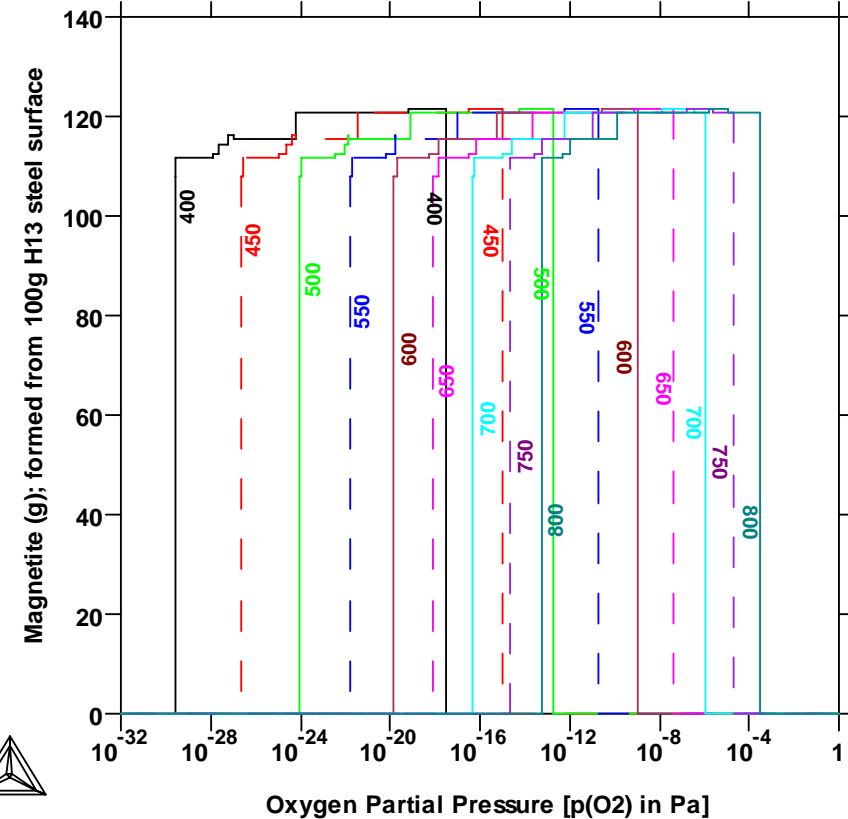
H13 Hot Work Steels: Phase Emergence with respect to Hematite



THERMO-CALC (2008.05.22:14.41) :

Databases: SSOL4+SSUB4

H13 Hot Work Steels: Emergence Condition with respect to Magnetite Phase



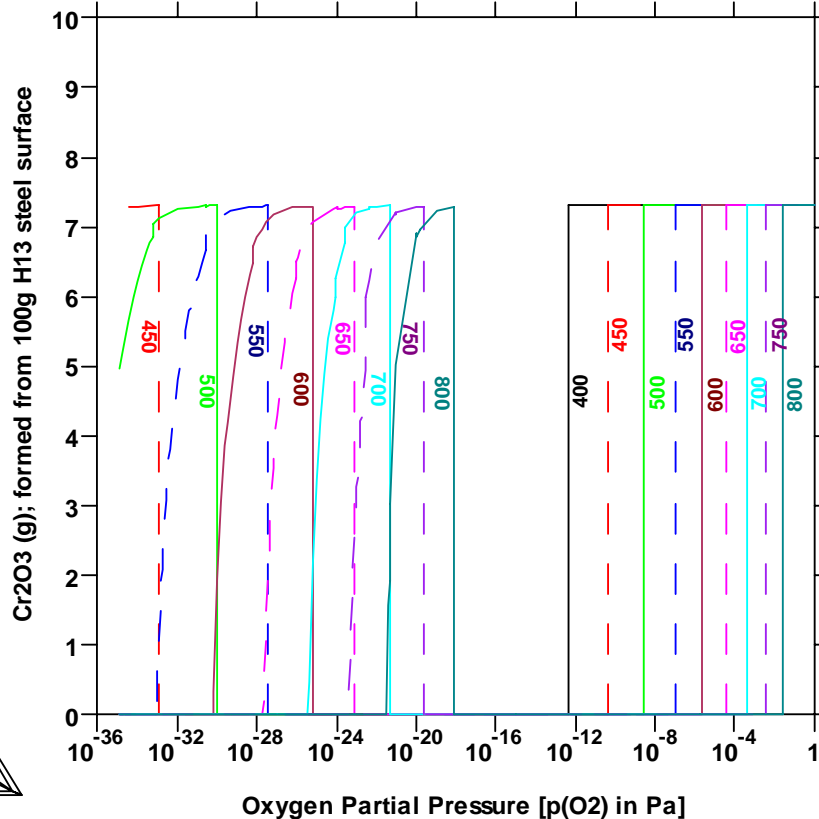
Emergence Conditions with respect to and Fe<sub>2</sub>O<sub>3</sub> (Hematite) and Fe<sub>3</sub>O<sub>4</sub> (Magnetite) during oxidation of H13 Hot Work Steel [Fe-5.14Cr-0.41Mn-1.02Si-0.40C-0.93V-1.46Mo-0.001S-0.009P-O], at 9 different temperatures (between 400 and 800°C, with an interval of 50°C) and 1 bar.

# Surface Redox Reactions (III)

## Example: Oxidation of H13 Hot Work Steel

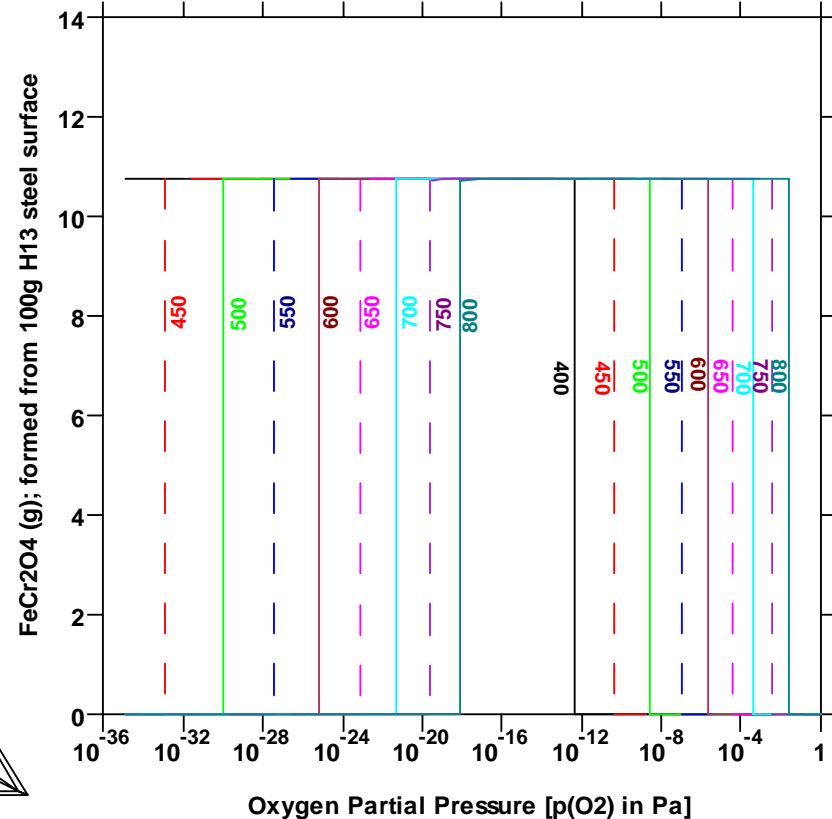
THERMO-CALC (2008.05.22:10.52) :  
Databases: SSOL4+SSUB4

H13 Hot Work Steels: Emergence Condition with respect to Cr<sub>2</sub>O<sub>3</sub> Phase



THERMO-CALC (2008.05.22:11.07) :  
Databases: SSOL4+SSUB4

H13 Hot Work Steels: Emergence Condition with respect to FeCr<sub>2</sub>O<sub>4</sub> Phase



Emergence Conditions with respect to Cr<sub>2</sub>O<sub>3</sub> and FeCr<sub>2</sub>O<sub>4</sub> during oxidation of H13 Hot Work Steel [Fe-5.14Cr-0.41Mn-1.02Si-0.40C-0.93V-1.46Mo-0.001S-0.009P-O], at 9 different temperatures (between 400 and 800°C, with an interval of 50°C) and 1 bar.

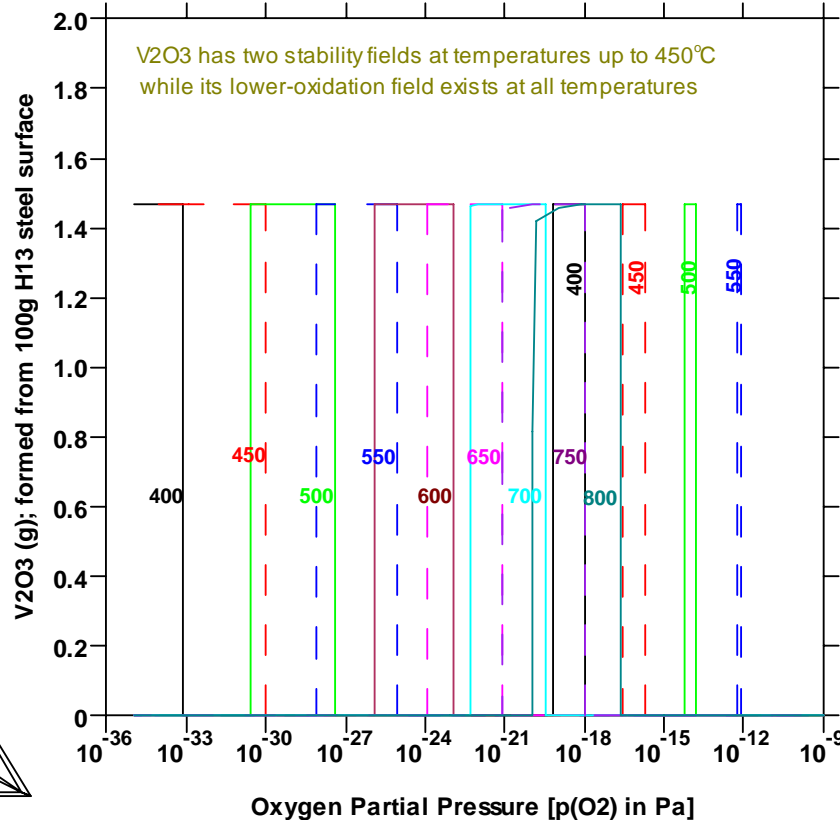
# Surface Redox Reactions (III)

## Example: Oxidation of H13 Hot Work Steel

THERMO-CALC (2008.05.22:11.50) :

Databases: SSOL4+SSUB4

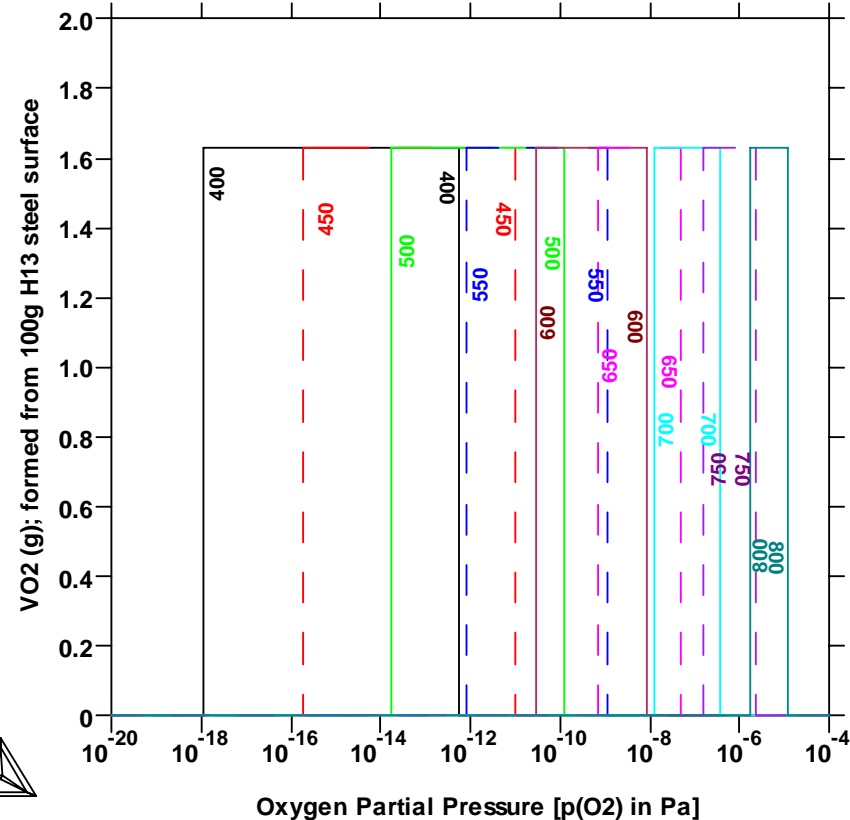
*H13 Hot Work Steels: Emergence Condition with respect to V<sub>2</sub>O<sub>3</sub> Phase*



THERMO-CALC (2008.05.22:14.15) :

Databases: SSOL4+SSUB4

*H13 Hot Work Steels: Emergence Condition with respect to VO<sub>2</sub> Phase*



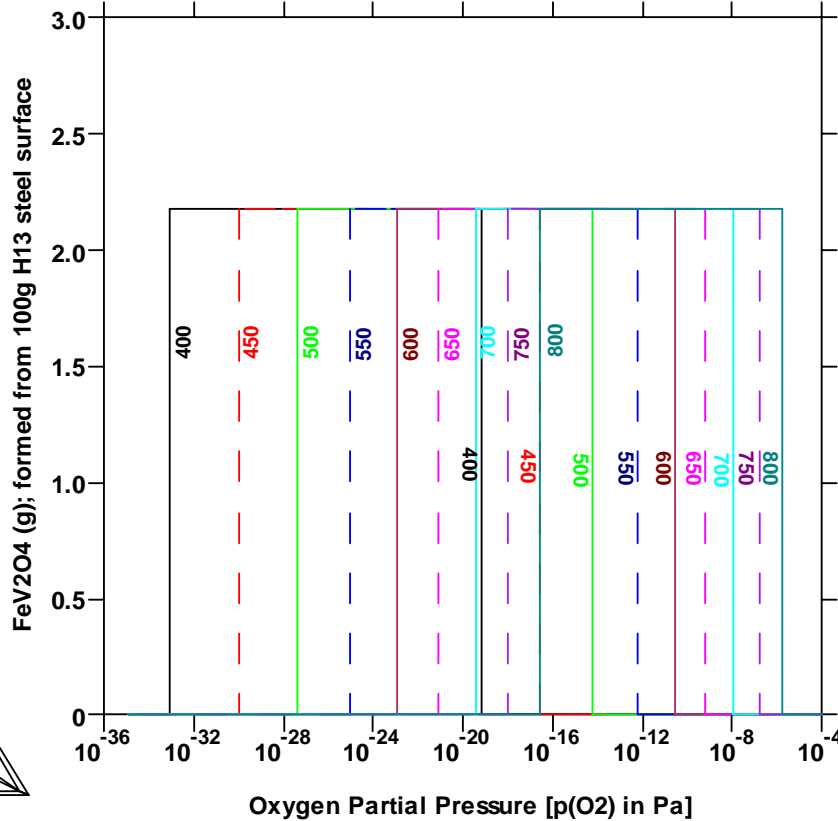
Emergence Conditions with respect to V<sub>2</sub>O<sub>3</sub> and VO<sub>2</sub> during oxidation of H13 Hot Work Steel [Fe-5.14Cr-0.41Mn-1.02Si-0.40C-0.93V-1.46Mo-0.001S-0.009P-O], at 9 different temperatures (between 400 and 800°C, with an interval of 50°C) and 1 bar.

# Surface Redox Reactions (III)

## Example: Oxidation of H13 Hot Work Steel

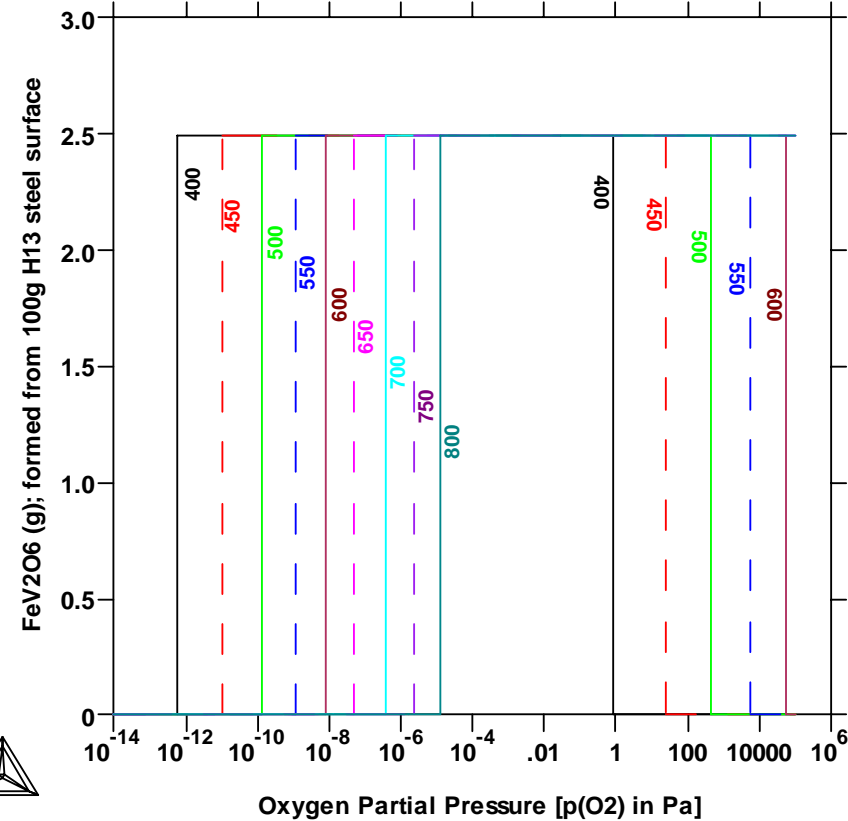
THERMO-CALC (2008.05.22:11.22) :  
Databases: SSOL4+SSUB4

*H13 Hot Work Steels: Emergence Condition with respect to FeV2O4 Phase*



THERMO-CALC (2008.05.22:15.45) :  
Databases: SSOL4+SSUB4

*H13 Hot Work Steels: Emergence Condition with respect to FeV2O6 Phase*



Emergence Conditions with respect to FeV<sub>2</sub>O<sub>4</sub> and FeV<sub>2</sub>O<sub>6</sub> during oxidation of H13 Hot Work Steel [Fe-5.14Cr-0.41Mn-1.02Si-0.40C-0.93V-1.46Mo-0.001S-0.009P-O], at 9 different temperatures (between 400 and 800°C, with an interval of 50°C) and 1 bar.

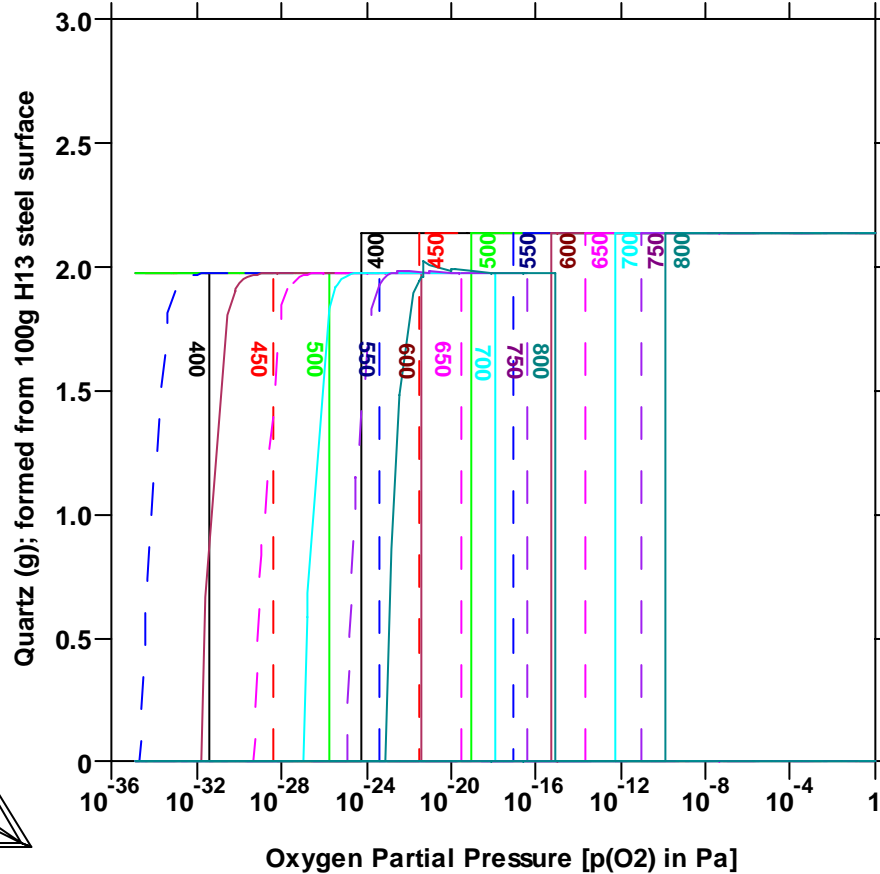
# Surface Redox Reactions (III)

## Example: Oxidation of H13 Hot Work Steel

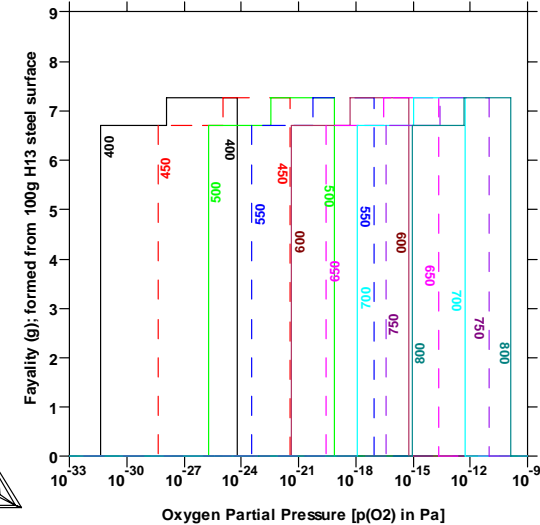
THERMO-CALC (2008.05.22:10.46) :

Databases: SSOL4+SSUB4

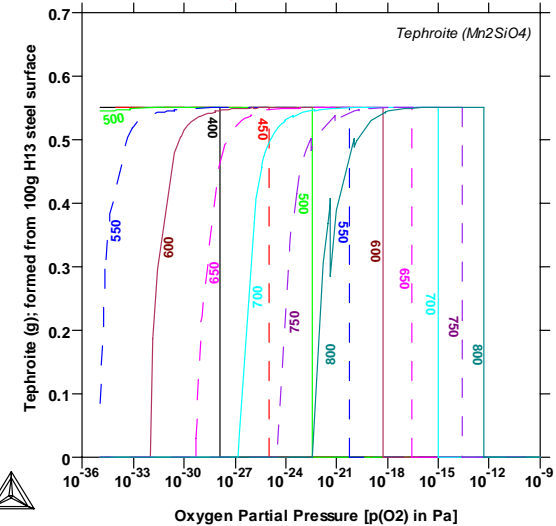
H13 Hot Work Steels: Emergence Condition with respect to  $\alpha/\beta$ -Quartz Phase



H13 Hot Work Steels: Emergence Condition with respect to Fayality Phase



H13 Hot Work Steels: Emergence Condition with respect to Tephroite Phase



Emergence Conditions with respect to SiO<sub>2</sub> ( $\alpha/\beta$ -Quartz), FeSiO<sub>4</sub> (Fayality) and MnSiO<sub>4</sub> (Tephroite) during oxidation of H13 Hot Work Steel [Fe-5.14Cr-0.41Mn-1.02Si-0.40C-0.93V-1.46Mo-0.001S-0.009P-O], at 9 different temperatures (between 400 and 800°C, with an interval of 50°C) and 1 bar.

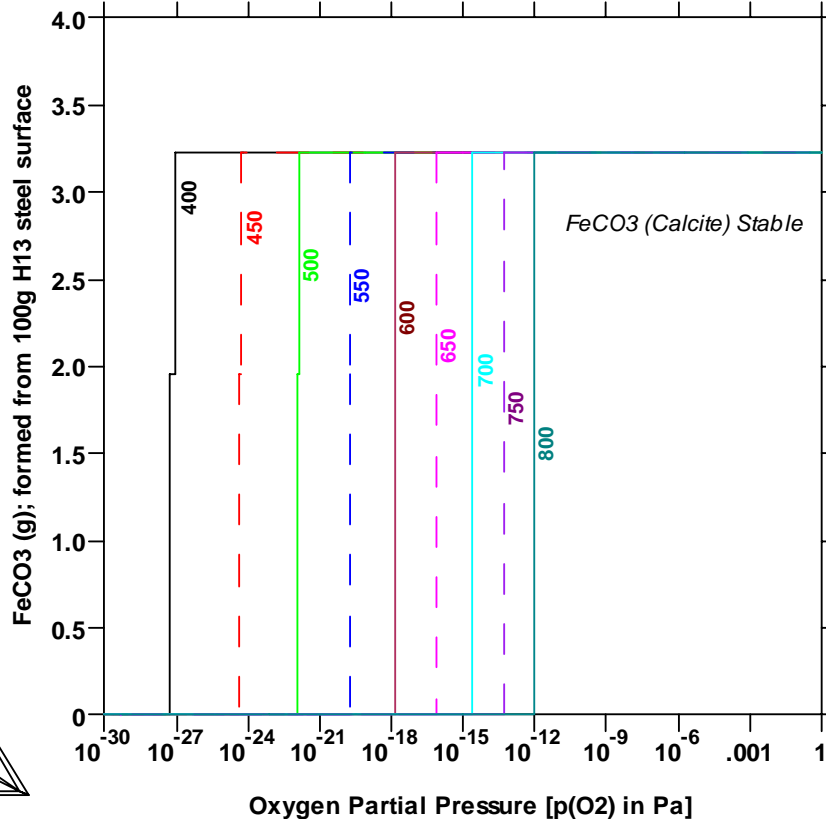
# Surface Redox Reactions (III)

## Example: Oxidation of H13 Hot Work Steel

THERMO-CALC (2008.05.22:15.18) :

Databases: SSOL4+SSUB4

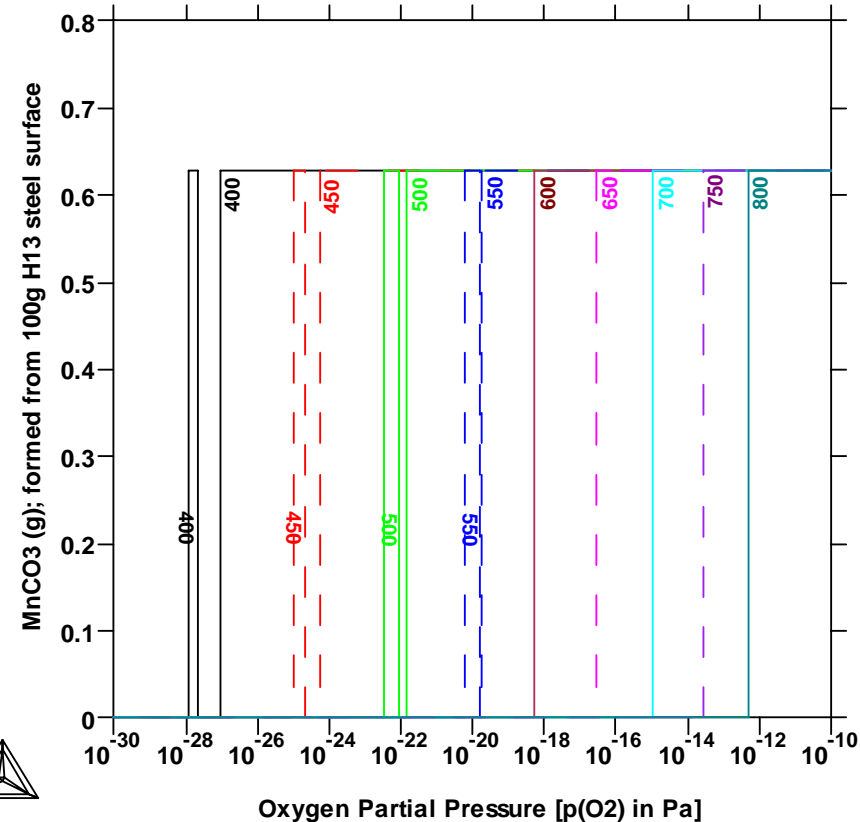
H13 Hot Work Steels: Emergence Condition with respect to FeCO<sub>3</sub> Phase



THERMO-CALC (2008.05.22:14.37) :

Databases: SSOL4+SSUB4

H13 Hot Work Steels: Emergence Condition with respect to MnCO<sub>3</sub> Phase



Emergence Conditions with respect to FeCO<sub>3</sub> (Calcite) and MnCO<sub>3</sub> during oxidation of H13 Hot Work Steel [Fe-5.14Cr-0.41Mn-1.02Si-0.40C-0.93V-1.46Mo-0.001S-0.009P-O], at 9 different temperatures (between 400 and 800°C, with an interval of 50°C) and 1 bar.